

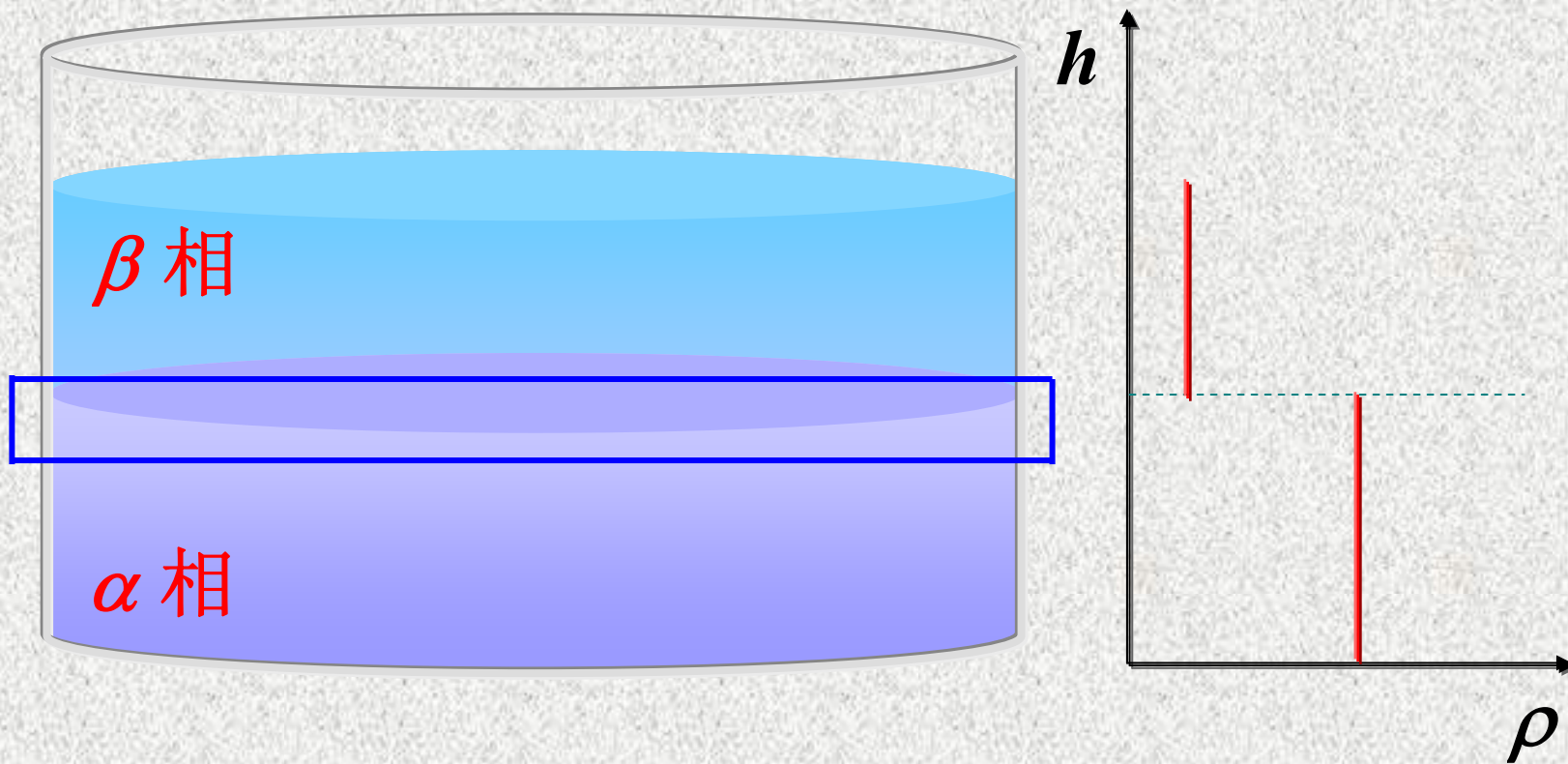
第十五章 界面现象

物理化学多媒体课堂教学软件 V1.0版

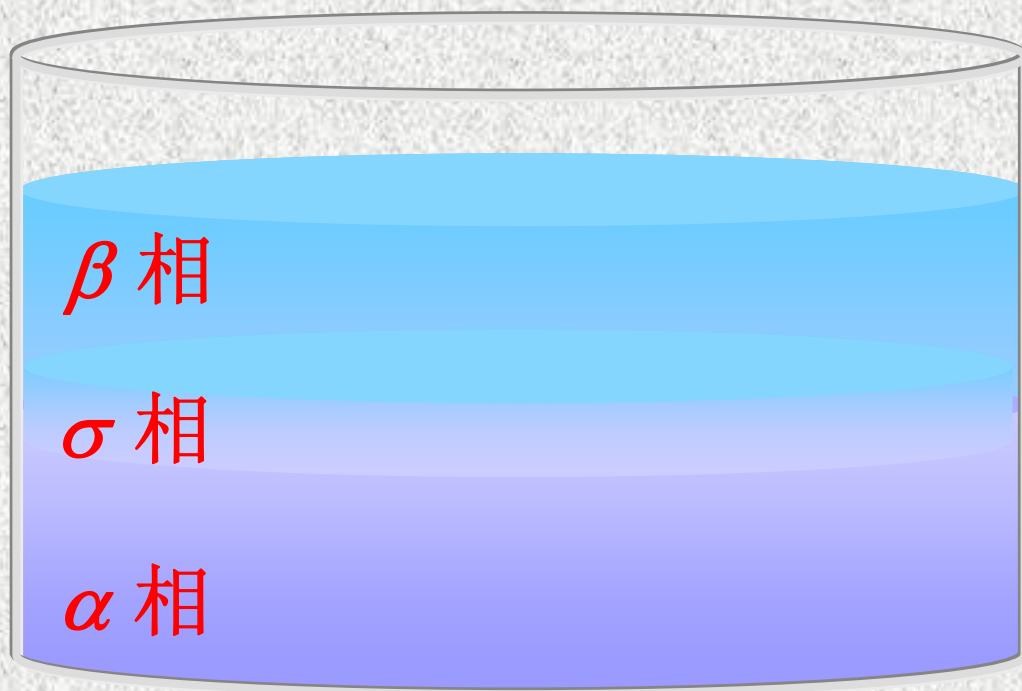
15-1 引言

物理化学多媒体课堂教学软件 V1.0版

界面与界相



界面与界相



界面现象

普遍规律

物质特性

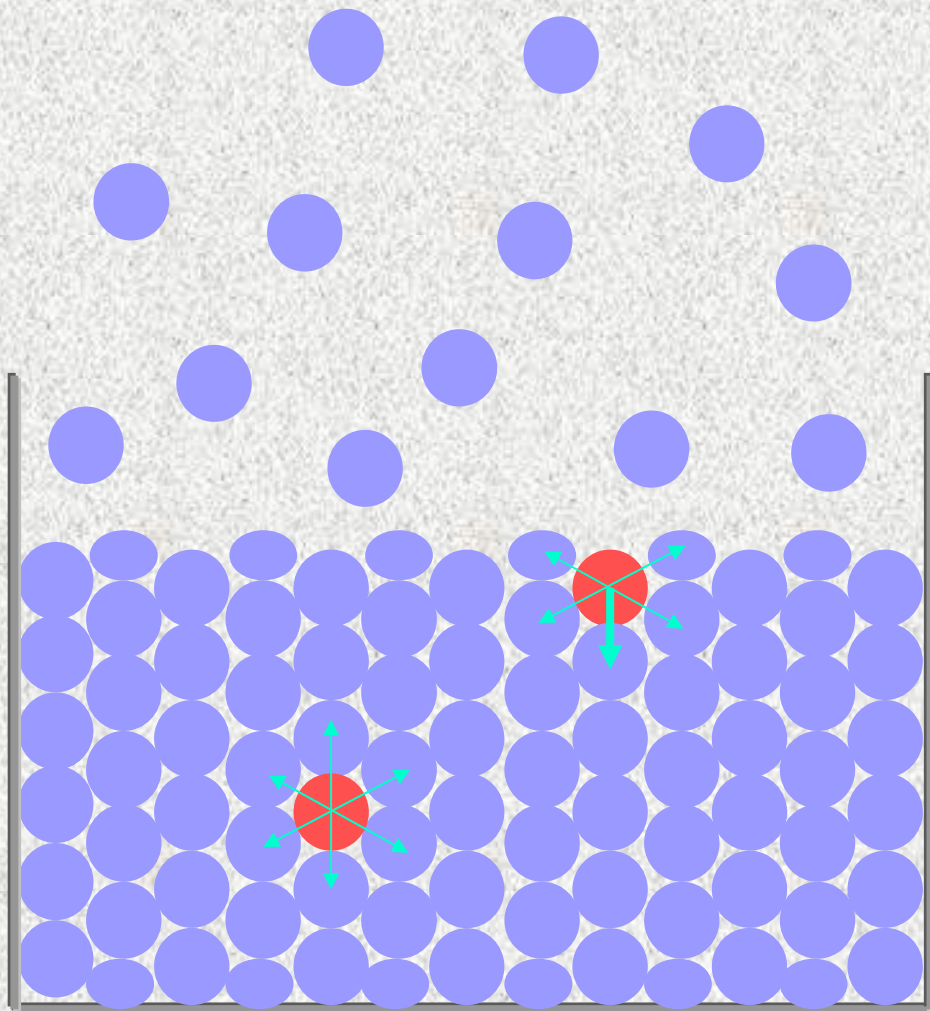
含界面相的热力学基本方程

界面张力
单位界面过剩量

15-2

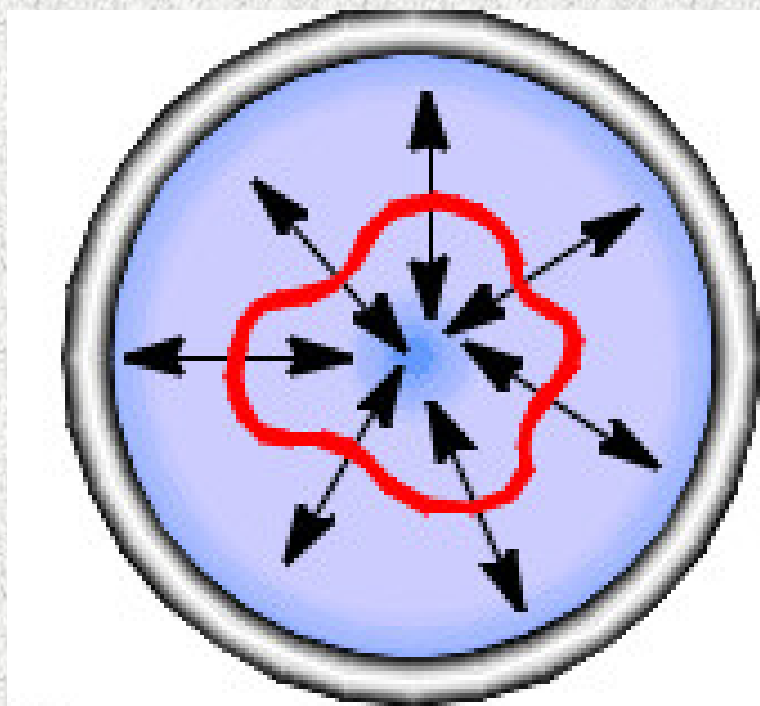
界面张力和界面过剩量

物理化学多媒体课堂教学软件 V1.0版

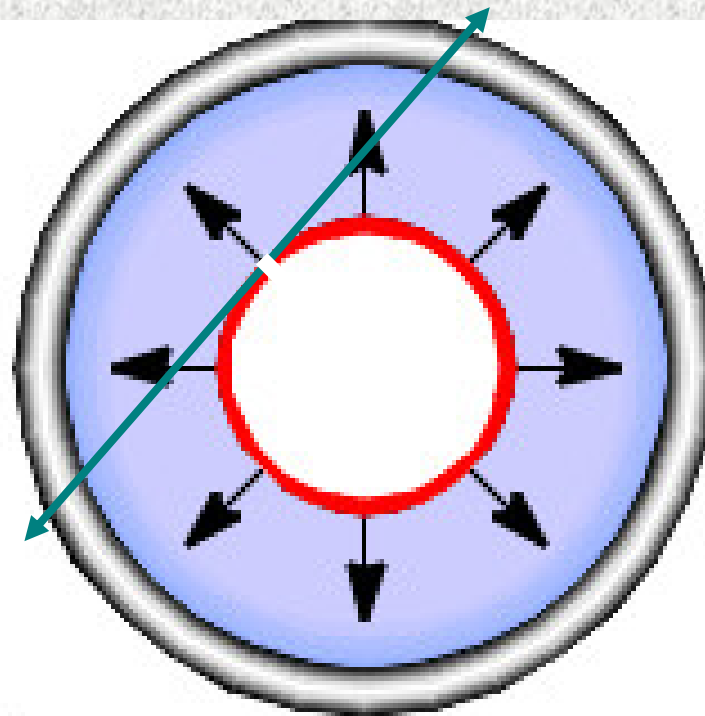


内压

单位面积界面层中的分子受到的指向体相内部并垂直于界面的引力

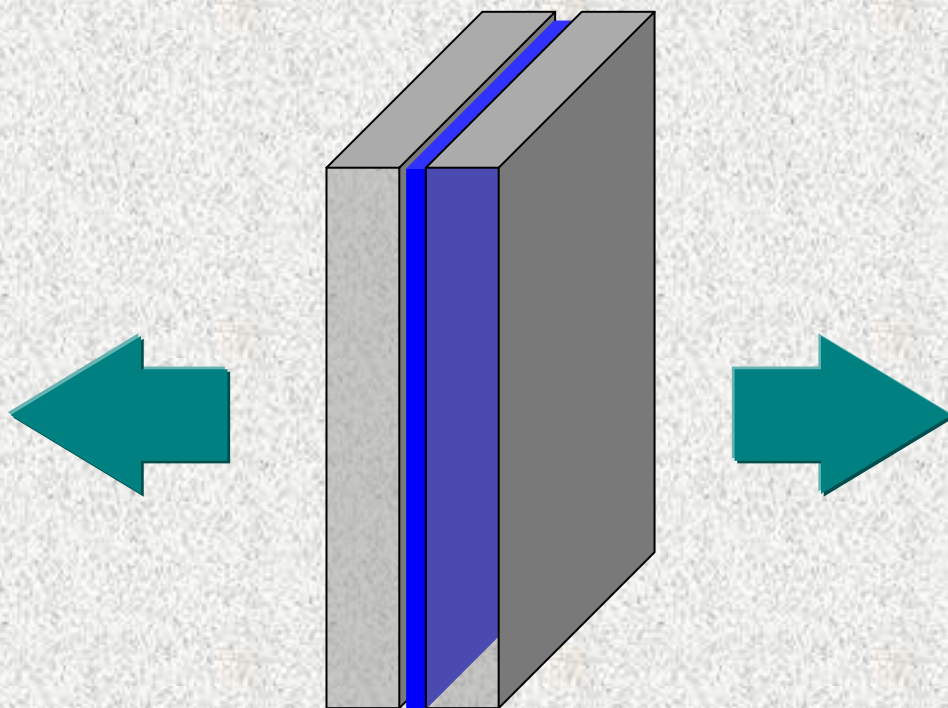


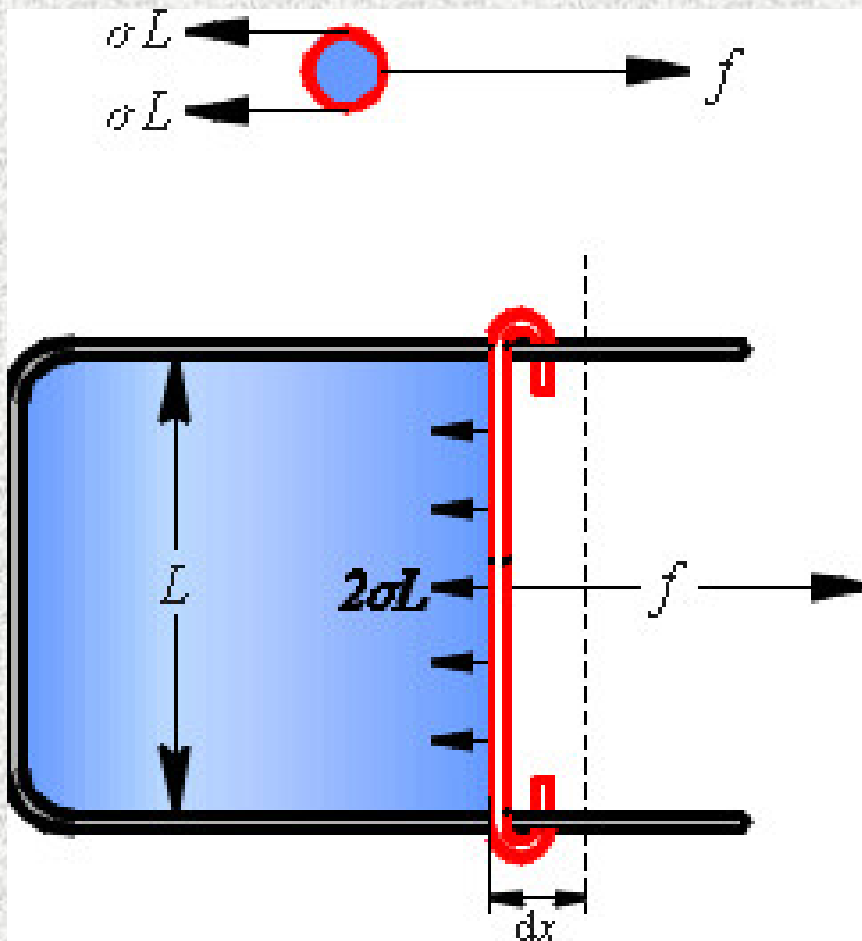
(a)



(b)

界面张力___界面中单位长度的收缩张力；它沿界面的切线方向作用于边缘上，并垂直于边缘。





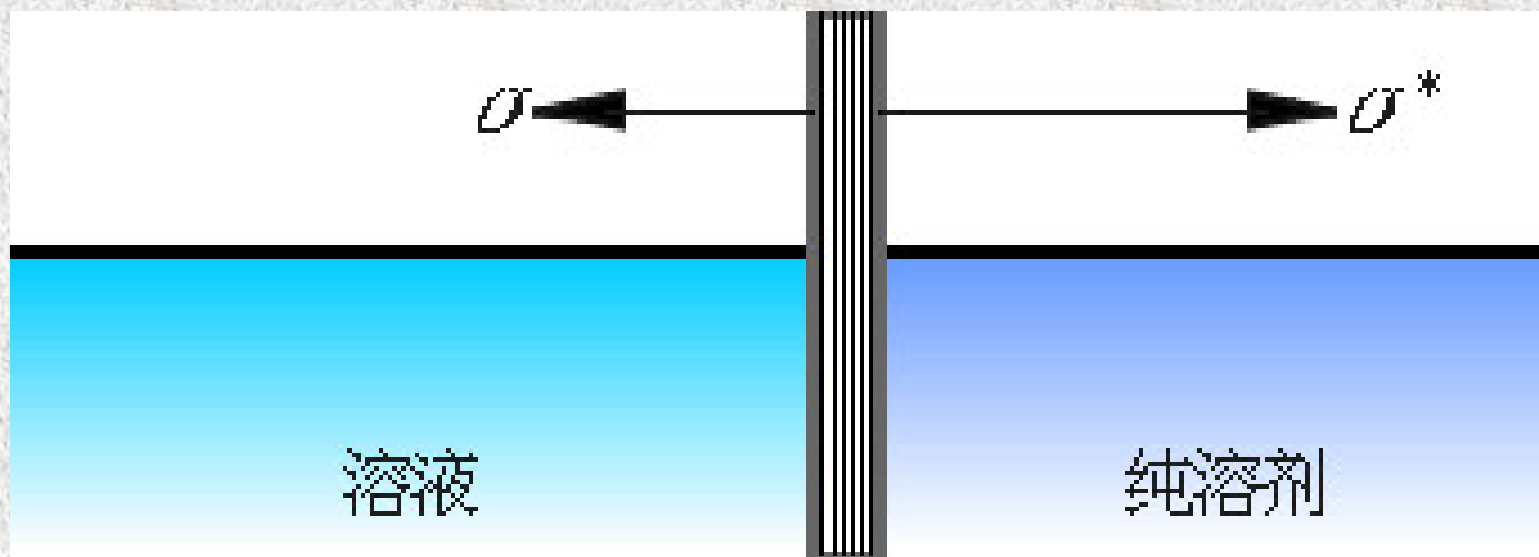
$$f = 2\sigma L$$

$$\begin{aligned} dW'_R &= f dx \\ &= 2\sigma L dx \\ &= \sigma dA_s \end{aligned}$$

$$\sigma = \frac{dW'_R}{dA_s}$$

界面张力____界面中单位长度的收缩张力；它沿界面的切线方向作用于边缘上，并垂直于边缘。

铺展压



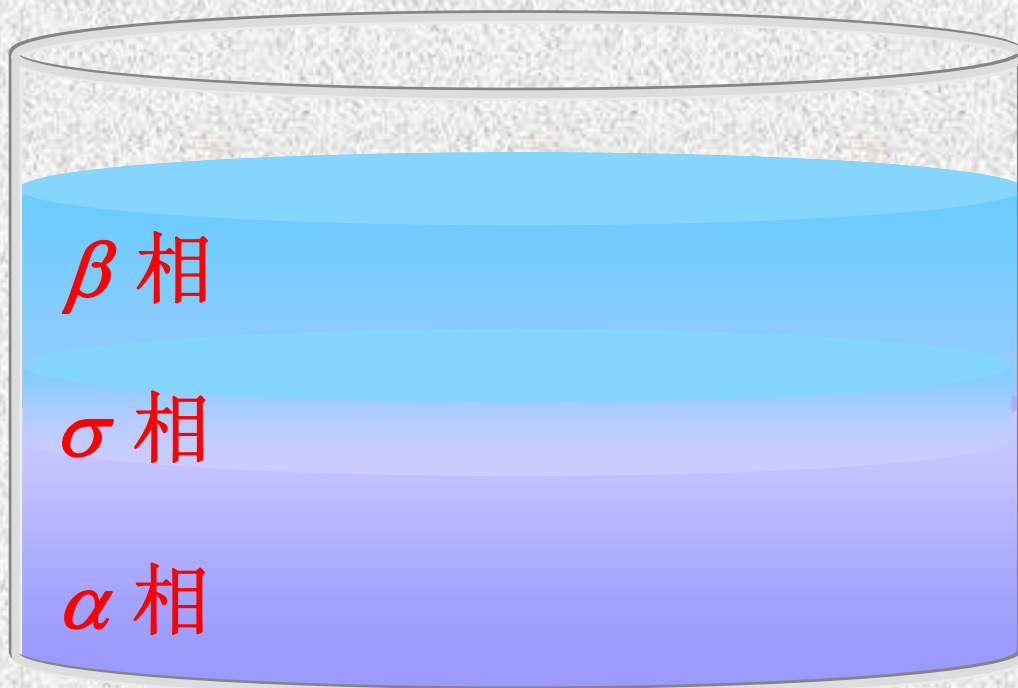
$$\pi \stackrel{\text{def}}{=} \sigma^* - \sigma$$

单位界面过剩量

$$n_i = n_i^{(\alpha)} + n_i^{(\beta)} + n_i^{(\sigma)}$$

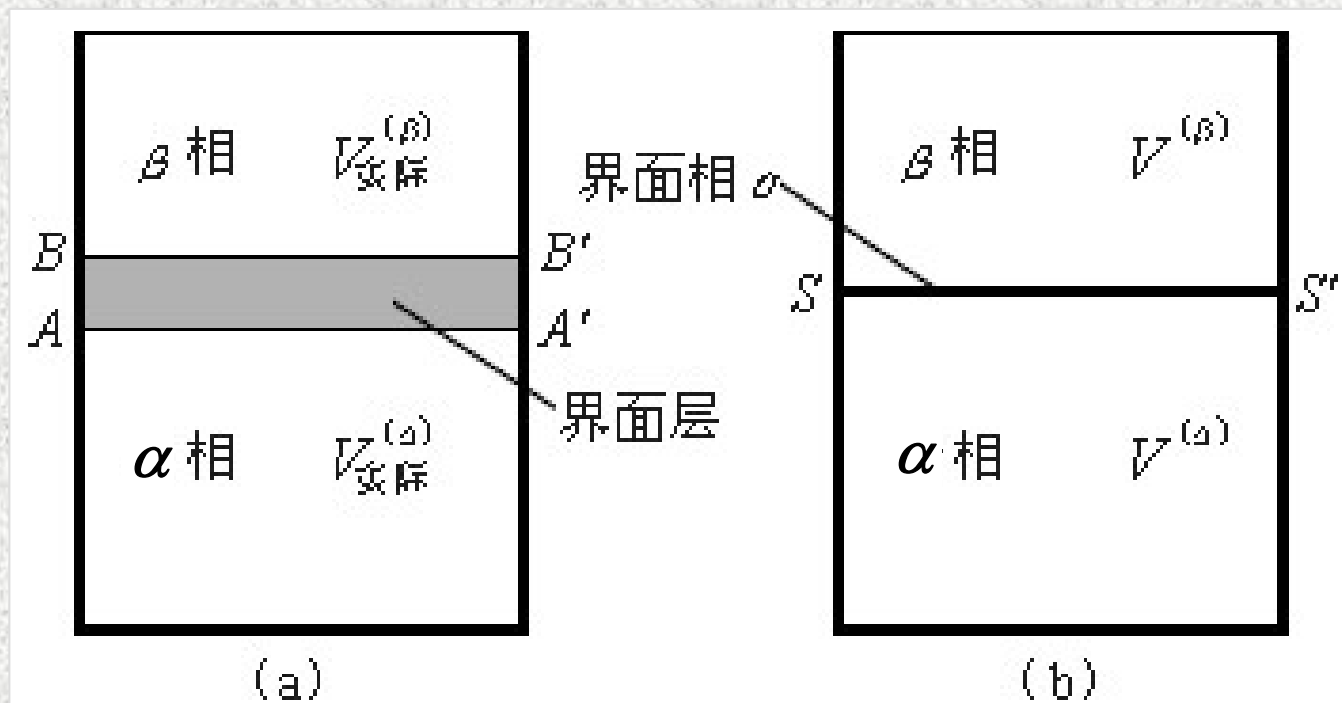
$$n_i^{(\alpha)} = c_i^{(\alpha)} V_{\text{实}}^{(\alpha)}$$

$$n_i^{(\beta)} = c_i^{(\beta)} V_{\text{实}}^{(\beta)}$$



吉布斯界面模型

- ◆ 将界面层抽象为无厚度无体积的平面界相，以符号 σ 表示
- ◆ 相和相的强度性质与实际系统中 α 相和 β 相的强度性质完全相同。 $\Delta = \Delta_{(\alpha)} + \Delta_{(\beta)}$



◆ 界面过剩量和单位界面过剩量

$$\begin{aligned}n_i^{(\sigma)} &\stackrel{\text{def}}{=} n_i - n_i^{(\alpha)} - n_i^{(\beta)} \\ &= n_i - V^{(\alpha)} c_i^{(\alpha)} - V^{(\beta)} c_i^{(\beta)}\end{aligned}$$

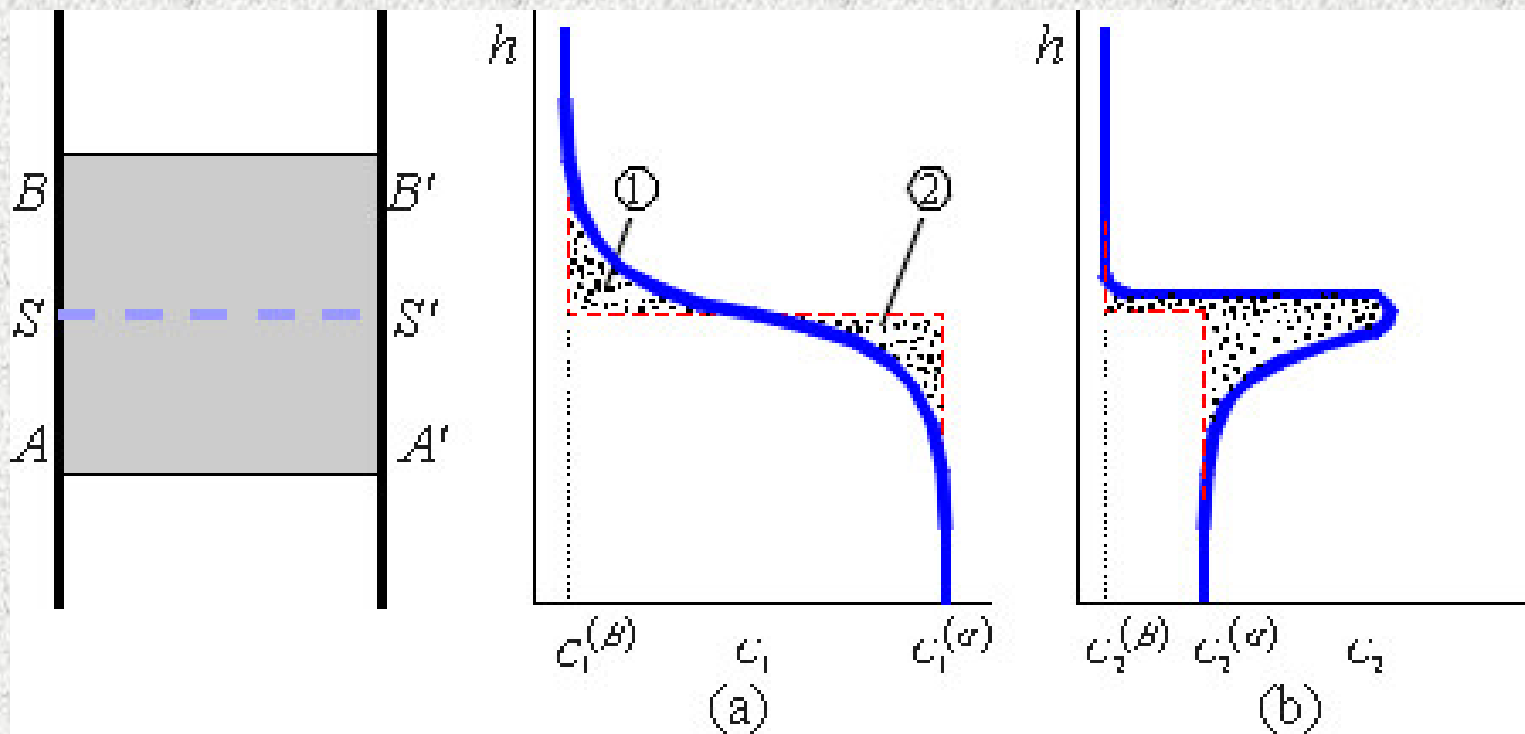
$$n_i^{(\sigma)} > 0 \quad \text{正吸附}$$

$$n_i^{(\sigma)} < 0 \quad \text{负吸附}$$

$$\Gamma_i \stackrel{\text{def}}{=} n_i^{(\sigma)} / A_s$$

◆ 吉布斯单位界面过剩量

$$\Gamma_i^{(1)} \stackrel{\text{def}}{=} \Gamma_i \quad (\Gamma_1 = 0) \quad \Gamma_1^{(1)} = 0$$



比表面 A_{s0}

——单位质量物质的表面积

$$A_{s0} \stackrel{\text{def}}{=} \frac{A_s}{m} = \frac{A_s}{\rho V}$$

15-3 热力学基本方程 和平衡条件

物理化学多媒体课堂教学软件 V1.0版

热力学第一、二定律

界面现象

考虑界面张力的热力学基本方程

考虑界面张力的平衡准则

弯曲界面
下的附加
压力

润湿
与
铺展

分散度对
蒸气压的
影响

吸附
平衡与
动力学

1.界面相的热力学基本方程

$$G^{(\sigma)} = G^{(\sigma)}(T^{(\sigma)}, p^{(\sigma)}, A_s, n_1^{(\sigma)}, n_2^{(\sigma)}, \dots, n_K^{(\sigma)})$$

$$dG^{(\sigma)} = -S^{(\sigma)}dT^{(\sigma)} + V^{(\sigma)}dp^{(\sigma)} + \left(\frac{\partial G^{(\sigma)}}{\partial A_s} \right)_{T, p, n_i} dA_s + \sum_{i=1}^K \mu_i^{(\sigma)} dn_i^{(\sigma)}$$

恒温恒压恒组成下 $dG = dW'_R$ $dW'_R = \sigma dA_s$

$$\sigma = \left(\frac{\partial G^{(\sigma)}}{\partial A_s} \right)_{T, p, n_i}$$

1.界面相的热力学基本方程

$$dU^{(\sigma)} = T^{(\sigma)}dS^{(\sigma)} - p^{(\sigma)}dV^{(\sigma)} + \sigma dA_s + \sum_i \mu_i^{(\sigma)} dn_i^{(\sigma)}$$

$$dH^{(\sigma)} = T^{(\sigma)}dS^{(\sigma)} + V^{(\sigma)}dp^{(\sigma)} + \sigma dA_s + \sum_i \mu_i^{(\sigma)} dn_i^{(\sigma)}$$

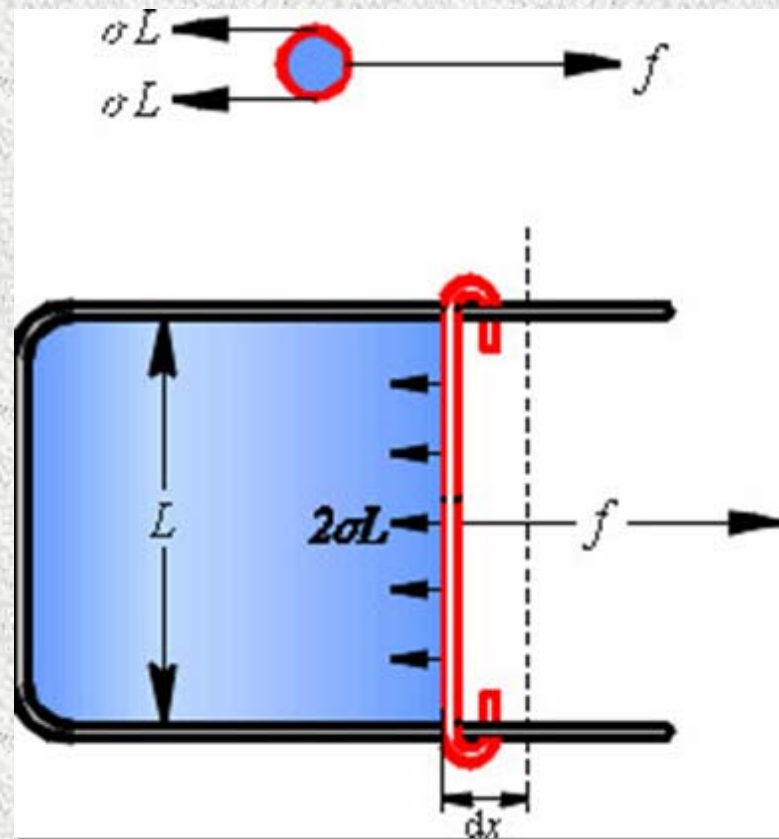
$$dA^{(\sigma)} = -S^{(\sigma)}dT^{(\sigma)} - p^{(\sigma)}dV^{(\sigma)} + \sigma dA_s + \sum_i \mu_i^{(\sigma)} dn_i^{(\sigma)}$$

$$dG^{(\sigma)} = -S^{(\sigma)}dT^{(\sigma)} + V^{(\sigma)}dp^{(\sigma)} + \sigma dA_s + \sum_i \mu_i^{(\sigma)} dn_i^{(\sigma)}$$

$$0 = S^{(\sigma)}dT^{(\sigma)} - V^{(\sigma)}dp^{(\sigma)} + A_s d\sigma + \sum_i n_i^{(\sigma)} d\mu_i^{(\sigma)}$$

界面张力__界面中单位长度的收缩张力；它沿界面的切线方向作用于边缘上，并垂直于边缘。

$$\sigma = \frac{dW'_R}{dA_s}$$



$$\sigma = \left(\frac{\partial U^{(\sigma)}}{\partial A_s} \right)_{S,V,n_j} = \left(\frac{\partial H^{(\sigma)}}{\partial A_s} \right)_{S,p,n_j} = \left(\frac{\partial A^{(\sigma)}}{\partial A_s} \right)_{T,V,n_j} = \left(\frac{\partial G^{(\sigma)}}{\partial A_s} \right)_{T,p,n_j}$$

包含界面相的热力学基本方程

设由两个体相 (α 、 β) 和一个界面相 σ 所组成的多相系统

$$X = X^{(\alpha)} + X^{(\beta)} + X^{(\sigma)}$$

$$dU = \sum_{\delta=\alpha,\beta,\sigma} \left(T^{(\delta)} dS^{(\delta)} - p^{(\delta)} dV^{(\delta)} + \sum_i \mu_i^{(\delta)} dn_i^{(\delta)} \right) + \sigma dA_s$$

$$dH = \sum_{\delta=\alpha,\beta,\sigma} \left(T^{(\delta)} dS^{(\delta)} + V^{(\delta)} dp^{(\delta)} + \sum_i \mu_i^{(\delta)} dn_i^{(\delta)} \right) + \sigma dA_s$$

$$dA = \sum_{\delta=\alpha,\beta,\sigma} \left(-S^{(\delta)} dT^{(\delta)} - p^{(\delta)} dV^{(\delta)} + \sum_i \mu_i^{(\delta)} dn_i^{(\delta)} \right) + \sigma dA_s$$

$$dG = \sum_{\delta=\alpha,\beta,\sigma} \left(-S^{(\delta)} dT^{(\delta)} + V^{(\delta)} dp^{(\delta)} + \sum_i \mu_i^{(\delta)} dn_i^{(\delta)} \right) + \sigma dA_s$$

$$0 = \sum_{\delta=\alpha,\beta,\sigma} \left(S^{(\delta)} dT^{(\delta)} - V^{(\delta)} dp^{(\delta)} + \sum_i n_i^{(\delta)} d\mu_i^{(\delta)} \right) + A_s d\sigma$$

2.有界面相时的平衡判据与平衡条件

❖ 平衡判据

热力学第一定律

$$dU = dQ + dW$$

$$dW = - \sum_{\delta=\alpha,\beta,\sigma} p^{(\delta)} dV^{(\delta)} + \sigma dA_s$$

热力学第二定律

$$\sum_{\delta=\alpha,\beta,\sigma} T^{(\delta)} dS^{(\delta)} - dQ \geq 0$$

$$dU = dQ + dW \leq \sum_{\alpha,\beta,\sigma} (T^{(\delta)} dS^{(\delta)} - p^{(\delta)} dV^{(\delta)}) + \sigma dA_s$$

2.有界面相时的平衡判据与平衡条件

❖ 平衡判据

$$dU \leq \sum_{\alpha, \beta, \sigma} (T^{(\delta)} dS^{(\delta)} - p^{(\delta)} dV^{(\delta)}) + \sigma dA_s$$

$$dU = \sum_{\delta=\alpha, \beta, \sigma} (T^{(\delta)} dS^{(\delta)} - p^{(\delta)} dV^{(\delta)} + \sum_i \mu_i^{(\delta)} dn_i^{(\delta)}) + \sigma dA_s$$

$$\sum_{\delta=\alpha, \beta, \sigma} \sum_i \mu_i^{(\delta)} dn_i^{(\delta)} \leq 0$$

有界面相时多相多组分
系统的平衡判据

2.有界面相时的平衡判据与平衡条件

❖ 平衡条件

• 平面界面的平衡条件

$$T^{(\alpha)} = T^{(\beta)} = T^{(\sigma)} = T$$

$$p^{(\alpha)} = p^{(\beta)} = p^{(\sigma)} = p$$

$$\mu_i^{(\alpha)} = \mu_i^{(\beta)} = \mu_i^{(\sigma)} = \mu_i$$

$$\sum_{\text{B}} \nu_{\text{B}} \mu_{\text{B}} = 0$$

2.有界面相时的平衡判据与平衡条件

❖ 平衡条件

• 弯曲界面的平衡条件

$$T^{(\alpha)} = T^{(\beta)} = T^{(\sigma)} = T$$

$$p^{(\alpha)} = p^{(\sigma)} = p^{(\beta)} + \sigma \left(dA_s / dV^{(\alpha)} \right)$$

$$\mu_i^{(\alpha)} = \mu_i^{(\beta)} = \mu_i^{(\sigma)} = \mu_i$$

$$\sum_B \nu_B \mu_B = 0$$

力平衡条件
变了!!!

15-4 拉普拉斯方程

物理化学多媒体课堂教学软件 V1.0版

❖ 存在弯曲界面时的力平衡条件

$$p^{(\alpha)} \quad p^{(\beta)} \quad p^{(\sigma)}$$

$$V^{(\alpha)} \quad V^{(\beta)} \quad V^{(\sigma)} = 0$$

$$dA = -p^{(\alpha)} dV^{(\alpha)}$$

$$- p^{(\beta)} dV^{(\beta)}$$

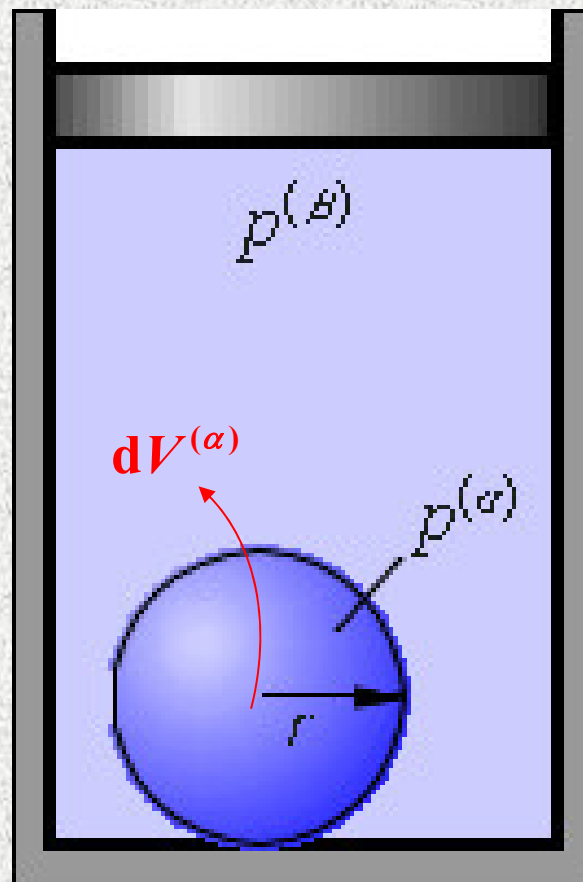
$$+ \sigma dA_s$$

$$= 0$$

$$dV^{(\alpha)} = -dV^{(\beta)}$$

$$dT = 0$$

$$dV = 0$$



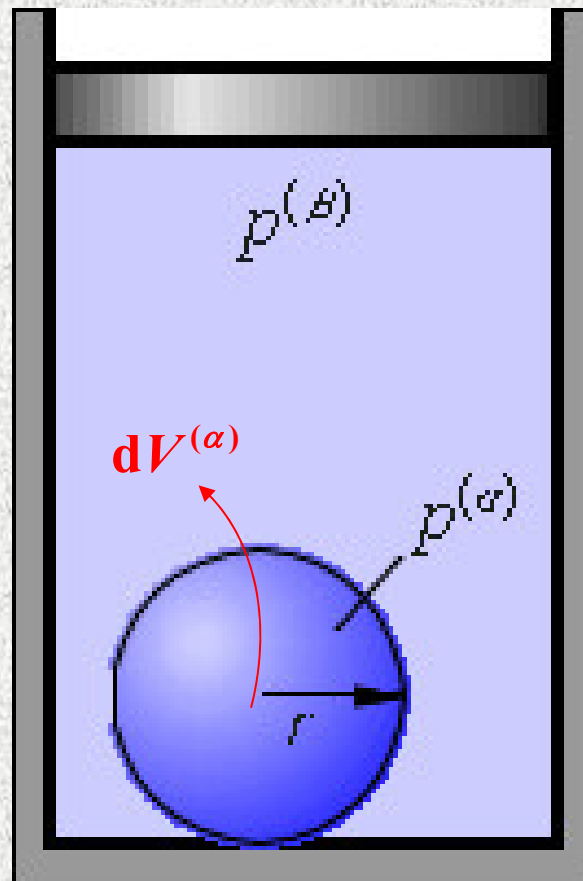
❖ 存在弯曲界面时的力平衡条件

$$p^{(\alpha)} \quad p^{(\beta)} \quad p^{(\sigma)}$$

$$V^{(\alpha)} \quad V^{(\beta)} \quad V^{(\sigma)} = 0$$

$$p^{(\alpha)} = p^{(\beta)} + \sigma \left(\frac{dA_s}{dV^{(\alpha)}} \right)$$

拉普拉斯方程



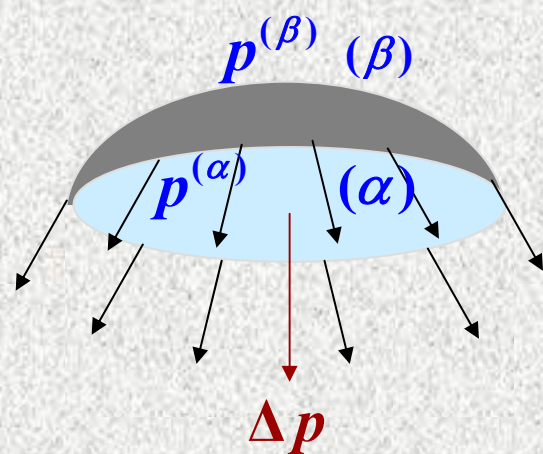
$$dT = 0 \quad dV = 0$$

❖ 附加压力 Δp

$$\sigma \left(\frac{dA_s}{dV^{(\alpha)}} \right)$$

$$\Delta p = p^{(\alpha)} - p^{(\beta)} = p_{(内)} - p_{(外)}$$

附加压力总是指向弯曲液面的曲率半径的中心



气相中的液滴

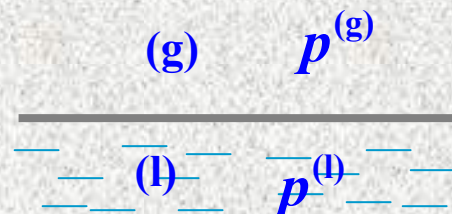
$$\Delta p = p^{(l)} - p^{(g)}$$

液相中的气泡

$$\Delta p = p^{(g)} - p^{(l)}$$

平面界面

$$p^{(g)} = p^{(l)}$$



$$p^{(\alpha)} = p^{(\beta)} + \sigma \left(\frac{dA_s}{dV^{(\alpha)}} \right)$$

球形液滴

非球形液滴

$$p^{(l)} = p^{(g)} + \frac{2\sigma}{r} \quad p^{(l)} = p^{(g)} + \sigma \left(\frac{1}{r_1} + \frac{1}{r_2} \right)$$

$$p^{(\alpha)} = p^{(\beta)} + \sigma \left(\frac{dA_s}{dV^{(\alpha)}} \right)$$

球形液滴

球形气泡

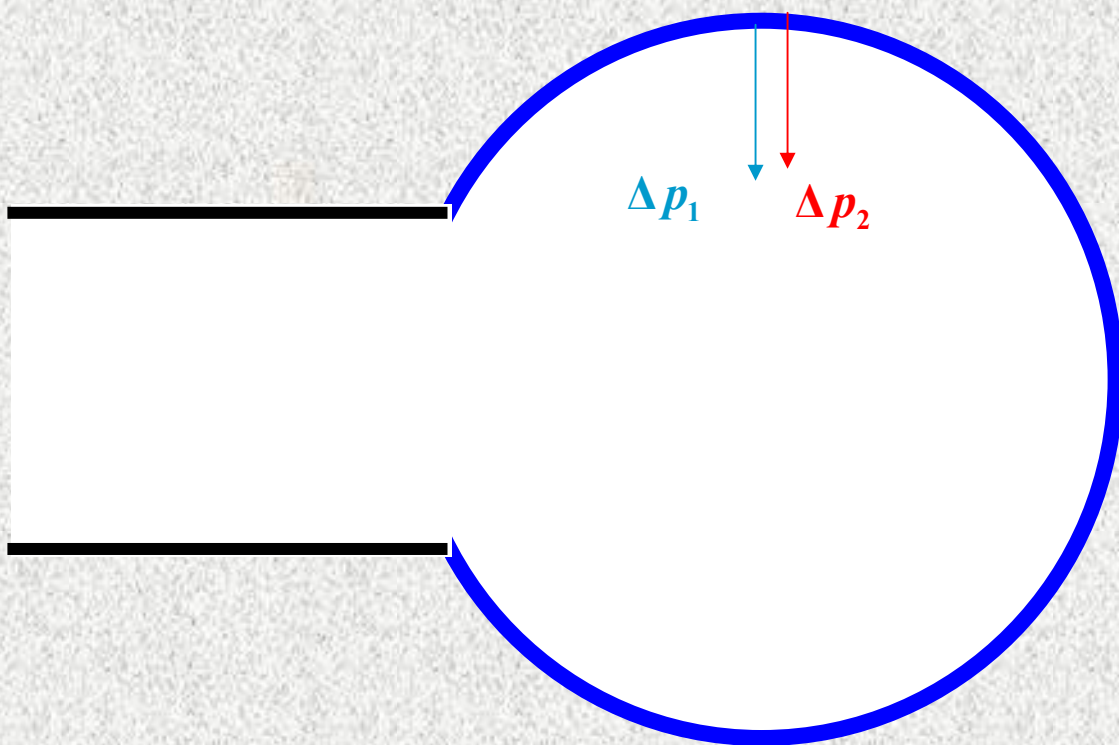
$$p^{(l)} = p^{(g)} + \frac{2\sigma}{r}$$

$$p^{(g)} = p^{(l)} + \frac{2\sigma}{r}$$

半径为 r 的球形弯曲液面

$$\Delta p = \frac{2\sigma}{r}$$

✦ 空气中的肥皂泡内外压差



$$\Delta p = 2 \times \frac{2\sigma}{r}$$

❖ 毛细管上升或下降

$$p_1^{(g)} + \rho^{(g)}gh$$

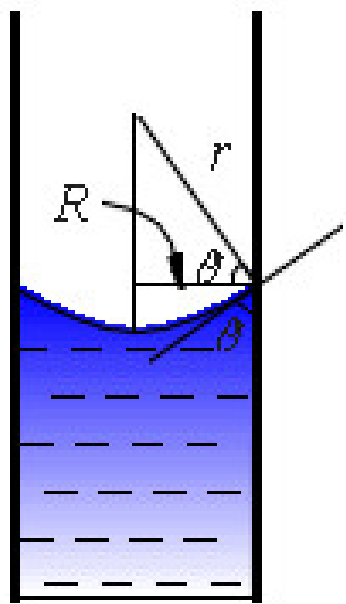
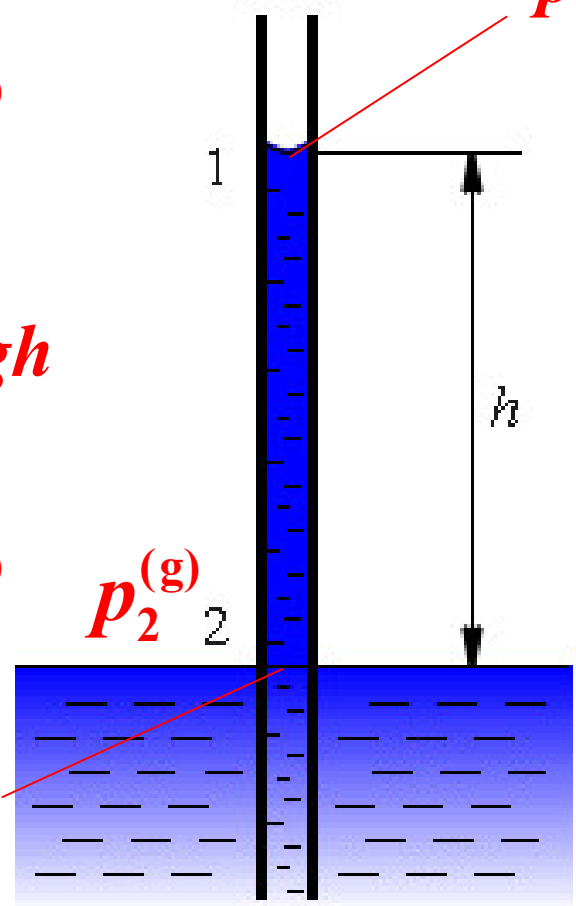
||

$$p_2^{(g)} \quad p_2^{(g)}$$

$$p_2^{(l)} = p_2^{(g)}$$

$$p_2^{(l)} = p_1^{(l)} + \rho^{(l)}gh \quad (a)$$

$$p_1^{(l)} = p_1^{(g)} - \frac{2\sigma}{r}$$



$$p_1^{(g)} - p_1^{(l)} = (\rho^{(l)} - \rho^{(g)})gh$$

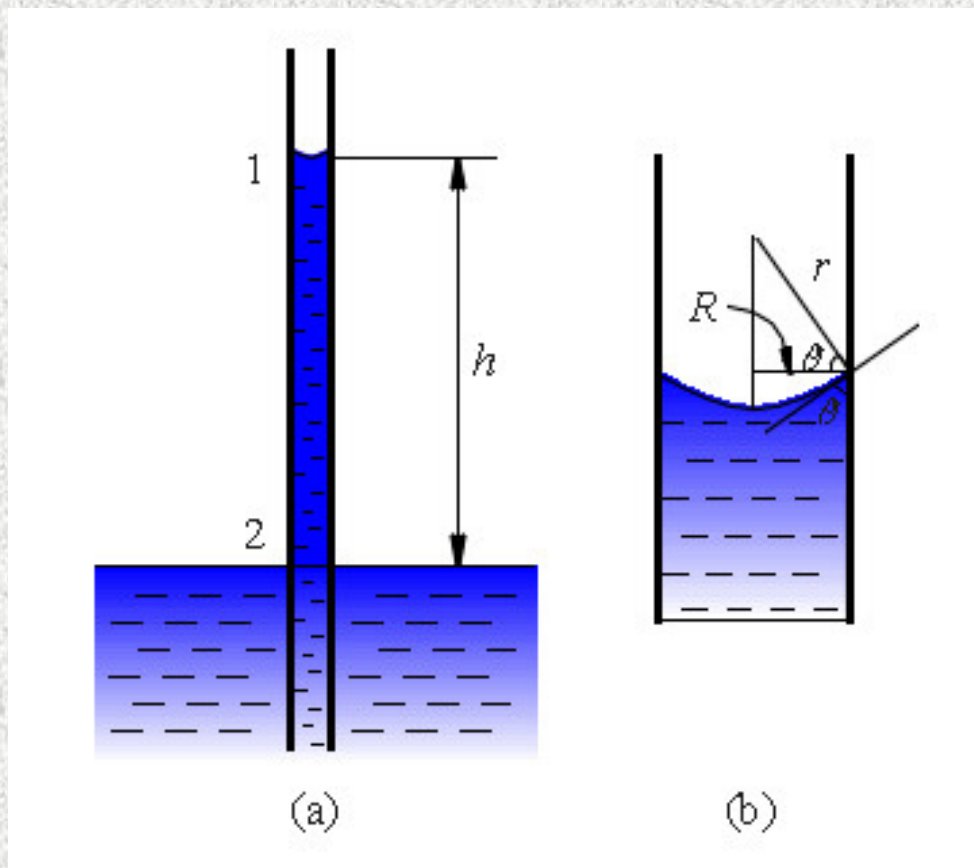
$$\frac{2\sigma}{r} = (\rho^{(g)} - \rho^{(l)})gh$$

❖ 毛细管上升或下降

$$\begin{aligned}\sigma &= \frac{r}{2} \rho^{(1)} gh \\ &= \frac{R}{2 \cos \theta} \rho^{(1)} gh\end{aligned}$$

因为 $\theta < 90^\circ$
 $\cos \theta > 0$

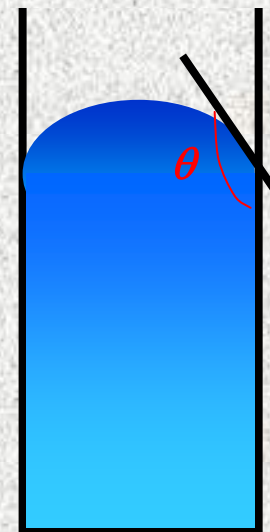
所以 $h > 0$



若液体能润湿毛细管，则在管内形成凹面，液面将上升

❖ 毛细管上升或下降

$$\begin{aligned}\sigma &= \frac{r}{2} \rho^{(1)} gh \\ &= \frac{R}{2 \cos \theta} \rho^{(1)} gh\end{aligned}$$



因为 $\theta > 90^\circ$ $\cos \theta < 0$

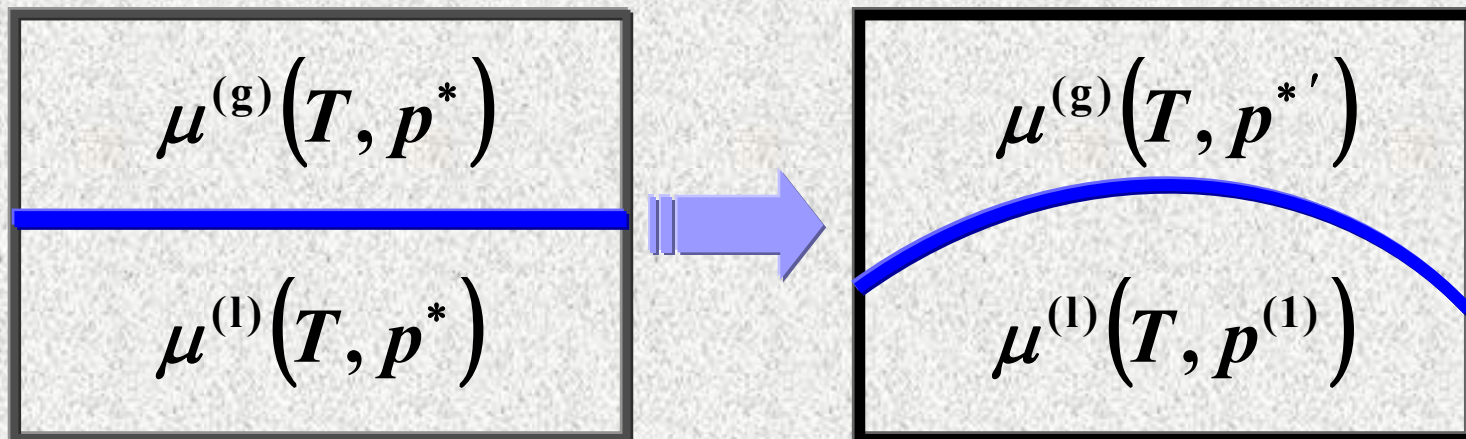
所以 $h < 0$

若液体不能润湿管壁，则在管内形成凸面，液面将下降

15-5 开尔文方程

物理化学多媒体课堂教学软件 V1.0版

1. 液体的饱和蒸气压随液体压力的变化



$$\mu^{(g)}(T, p^{*'}) - \mu^{(g)}(T, p^*) = \mu^{(l)}(T, p^{(l)}) - \mu^{(l)}(T, p^*)$$

$$d\mu = V_m dp \quad \int_{p^*}^{p^{*'}} V_m^{(g)} dp^{(g)} = \int_{p^*}^{p^{(l)}} V_m^{(l)} dp^{(l)} \quad V_m^{(g)} = \frac{RT}{p^{(g)}}$$

$$RT \ln \frac{p^{*'}}{p^*} = V_m^{(l)} (p^{(l)} - p^*)$$

2. 液体的饱和蒸气压随表面曲率的变化

凸面液体

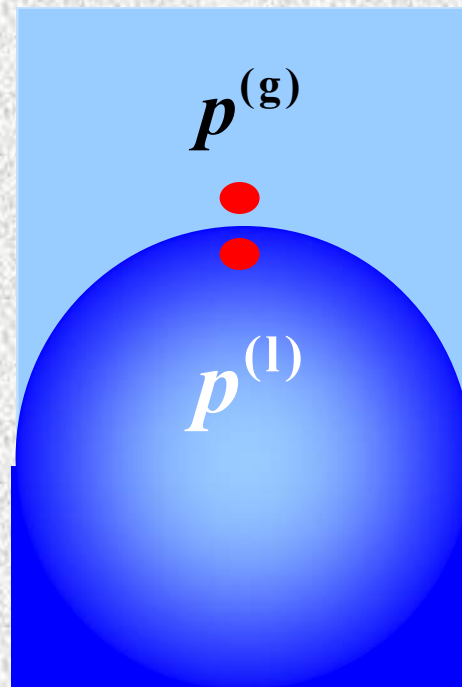
$$p^{(l)} = p^{(g)} + \frac{2\sigma}{r} = p_r^* + \frac{2\sigma}{r}$$

$$RT \ln \frac{p_r^*}{p^*} = V_m^{(l)} \left(p_r^* + \frac{2\sigma}{r} - p^* \right)$$

$$\approx V_m^{(l)} \frac{2\sigma}{r} = \frac{2\sigma M}{\rho r}$$

$$\ln \frac{p_r^*}{p^*} = \frac{2\sigma M}{RT \rho r}$$

开尔文方程



2. 液体的饱和蒸气压随表面曲率的变化

凹面液体

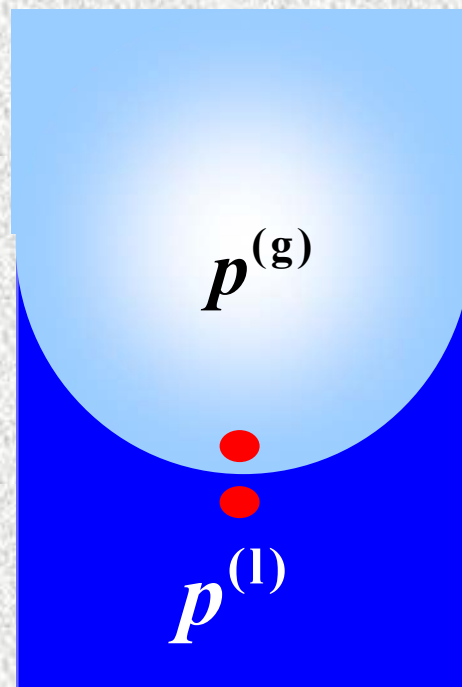
$$p^{(l)} = p^{(g)} - \frac{2\sigma}{r} = p_r^* - \frac{2\sigma}{r}$$

$$RT \ln \frac{p_r^*}{p^*} = V_m^{(l)} \left(p_r^* - \frac{2\sigma}{r} - p^* \right)$$

$$\approx -V_m^{(l)} \frac{2\sigma}{r} = -\frac{2\sigma M}{\rho r}$$

$$\ln \frac{p_r^*}{p^*} = -\frac{2\sigma M}{RT\rho r}$$

开尔文方程



液体中的气泡

弯曲液面对液体饱和蒸气压的影响，其实质是液体压力对液体饱和蒸气压的影响。

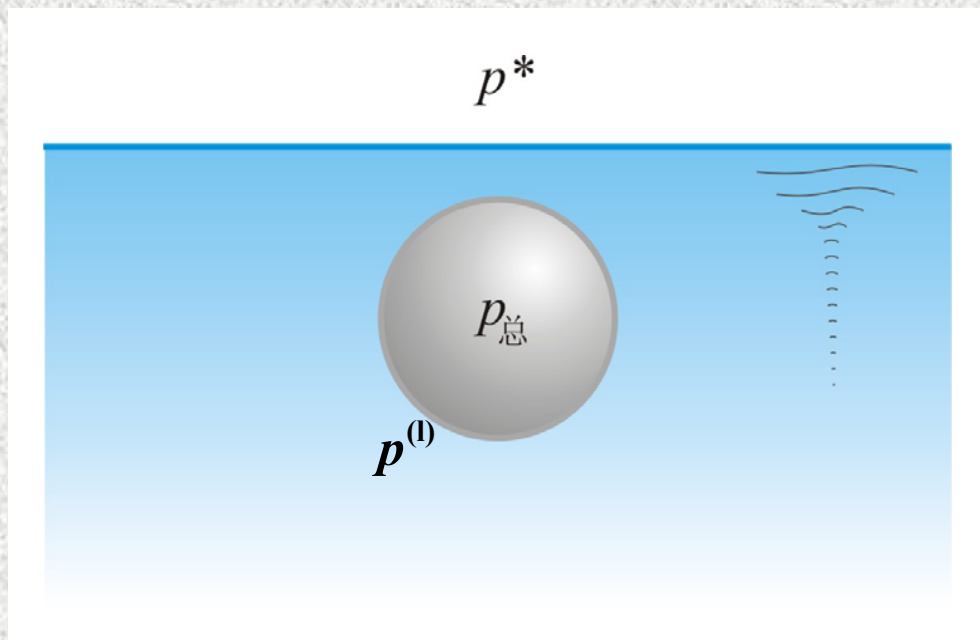
$$RT \ln \frac{p_r^*}{p^*} = V_m^{(l)} (p^{(l)} - p^*)$$

$$p_r^* = p^* \frac{p^{(l)}}{p^*} \quad p^{(l)} = p_{\text{外}}$$

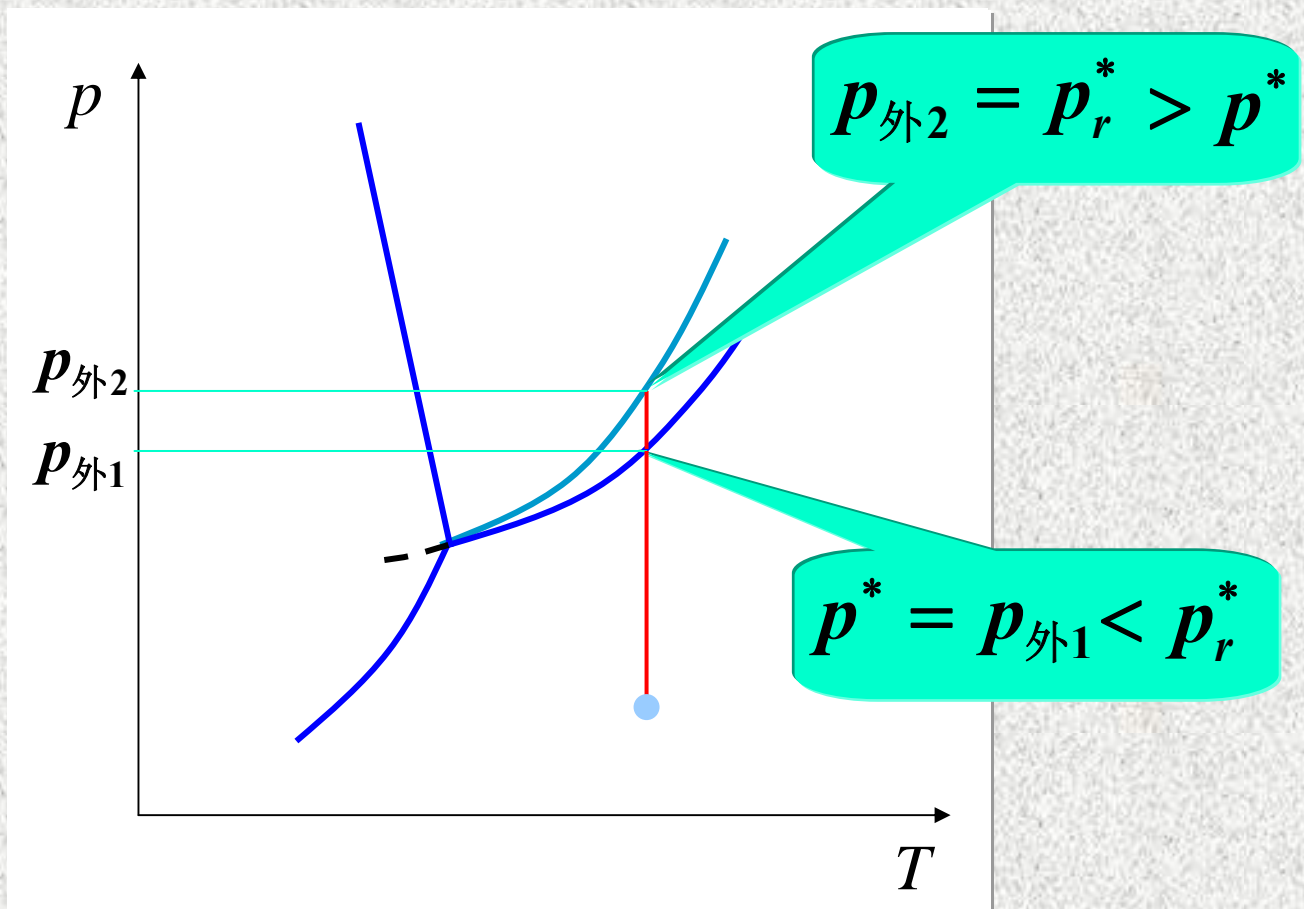
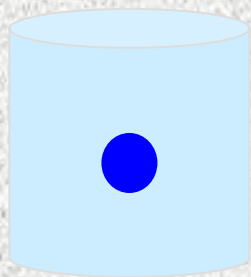
$$p^{(g)} = p^{(l)} + \frac{2\sigma}{r}$$

$$p_r^* = p^* + \frac{2\sigma}{r}$$

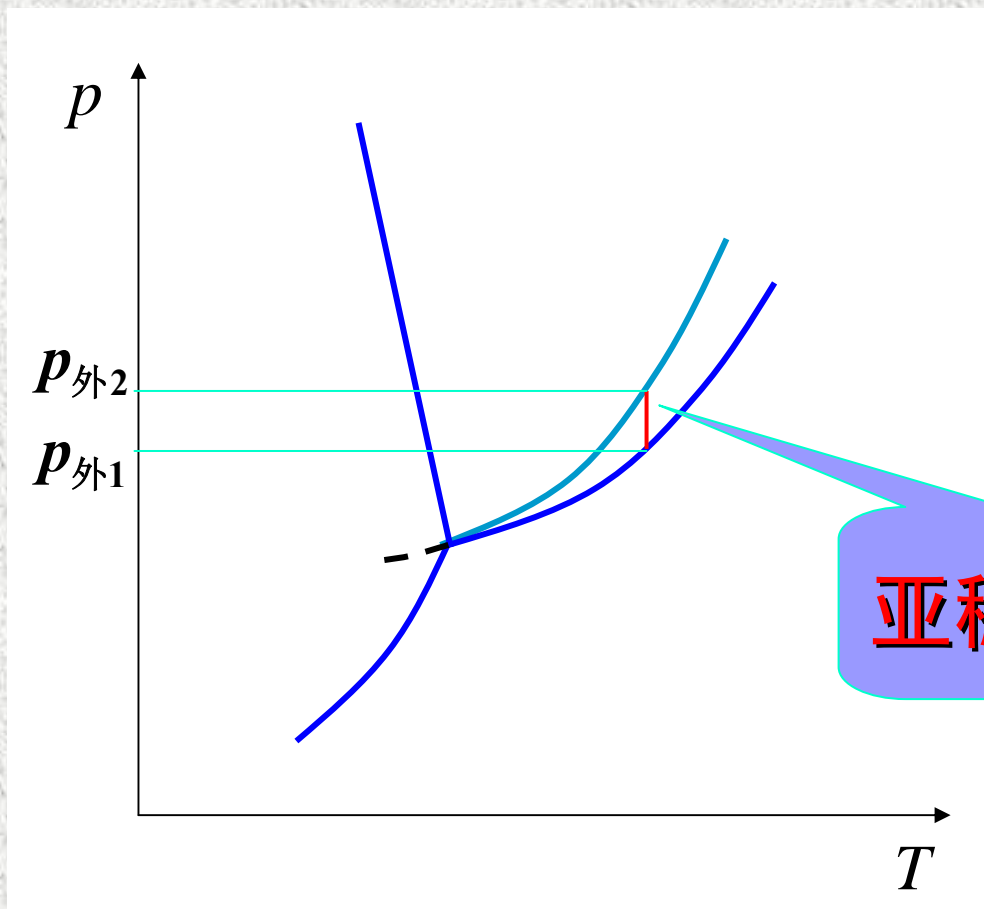
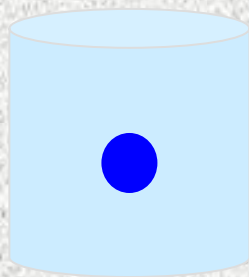
$$= p_{\text{总}}$$



过饱和蒸气

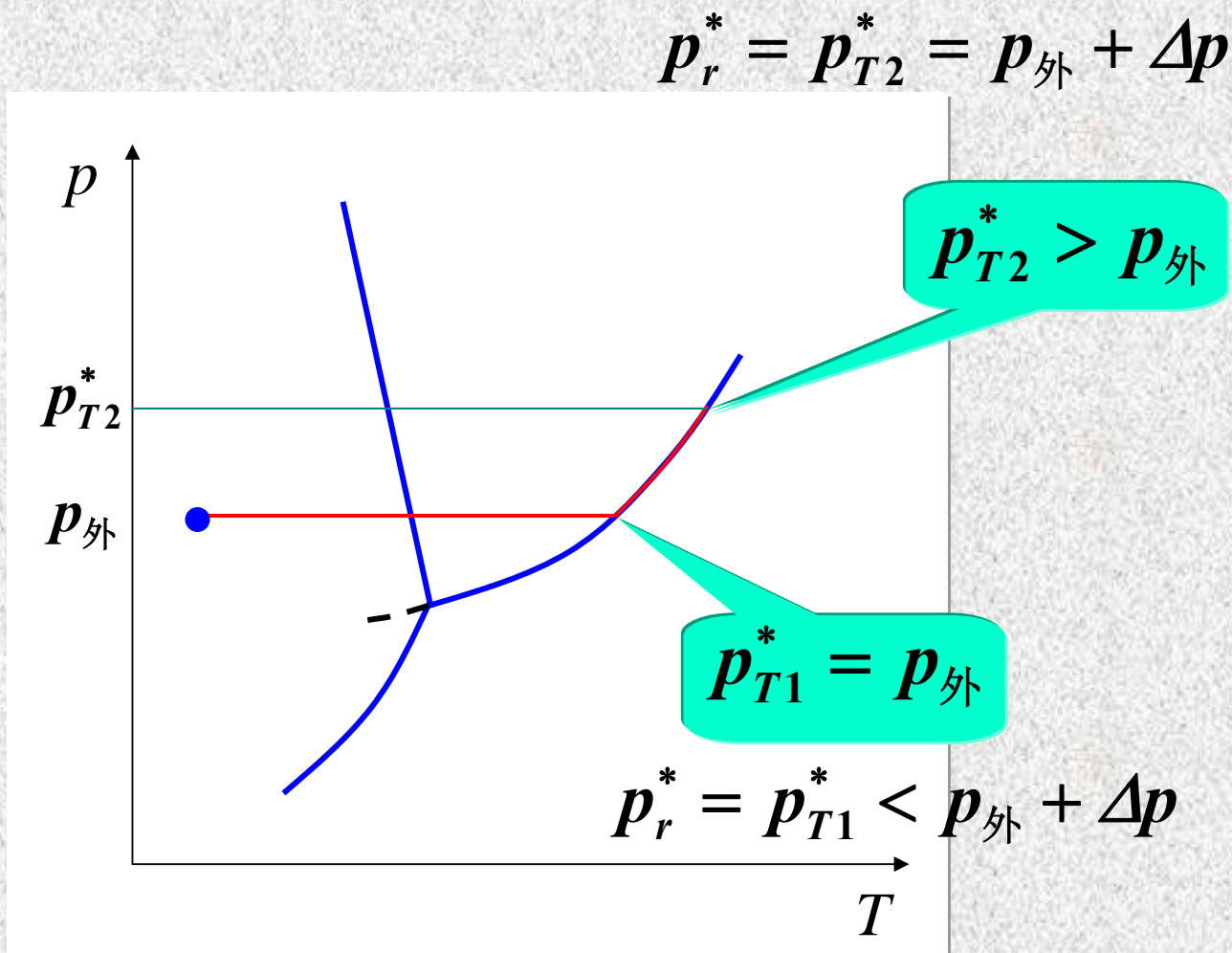
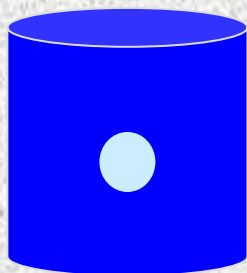


过饱和蒸气

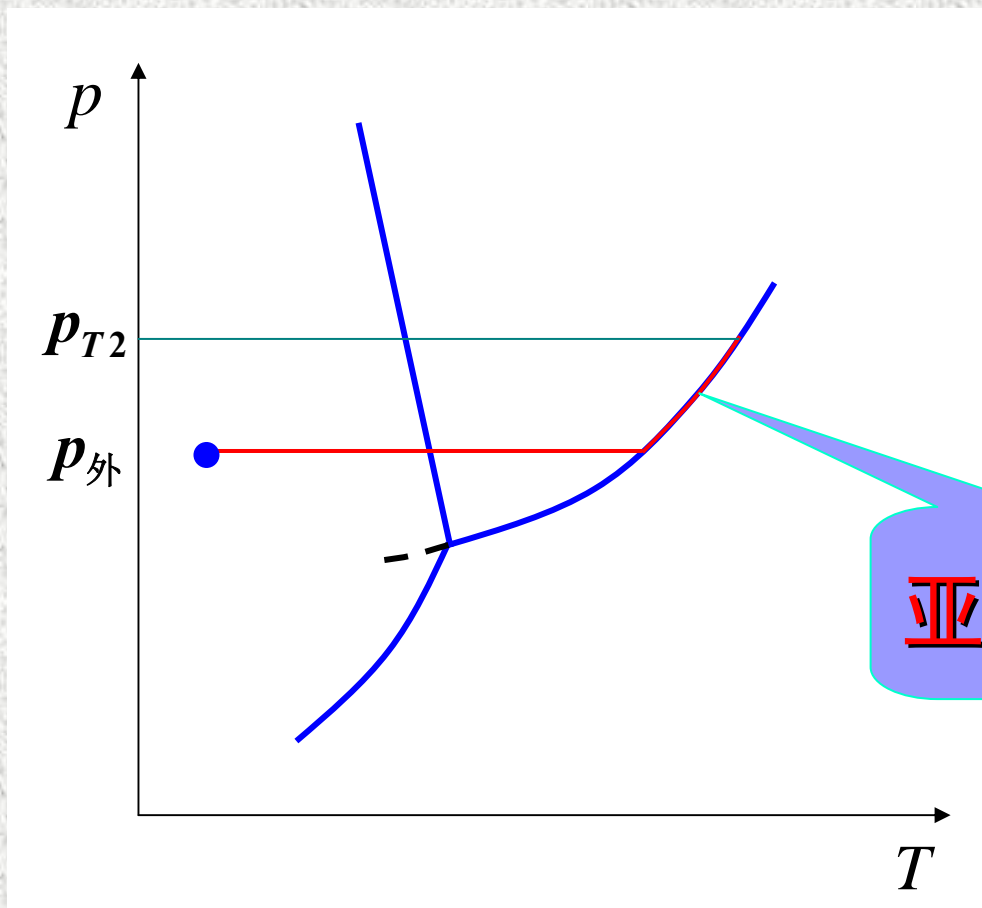
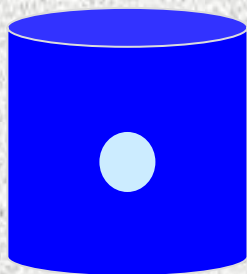


亚稳状态

过热液体

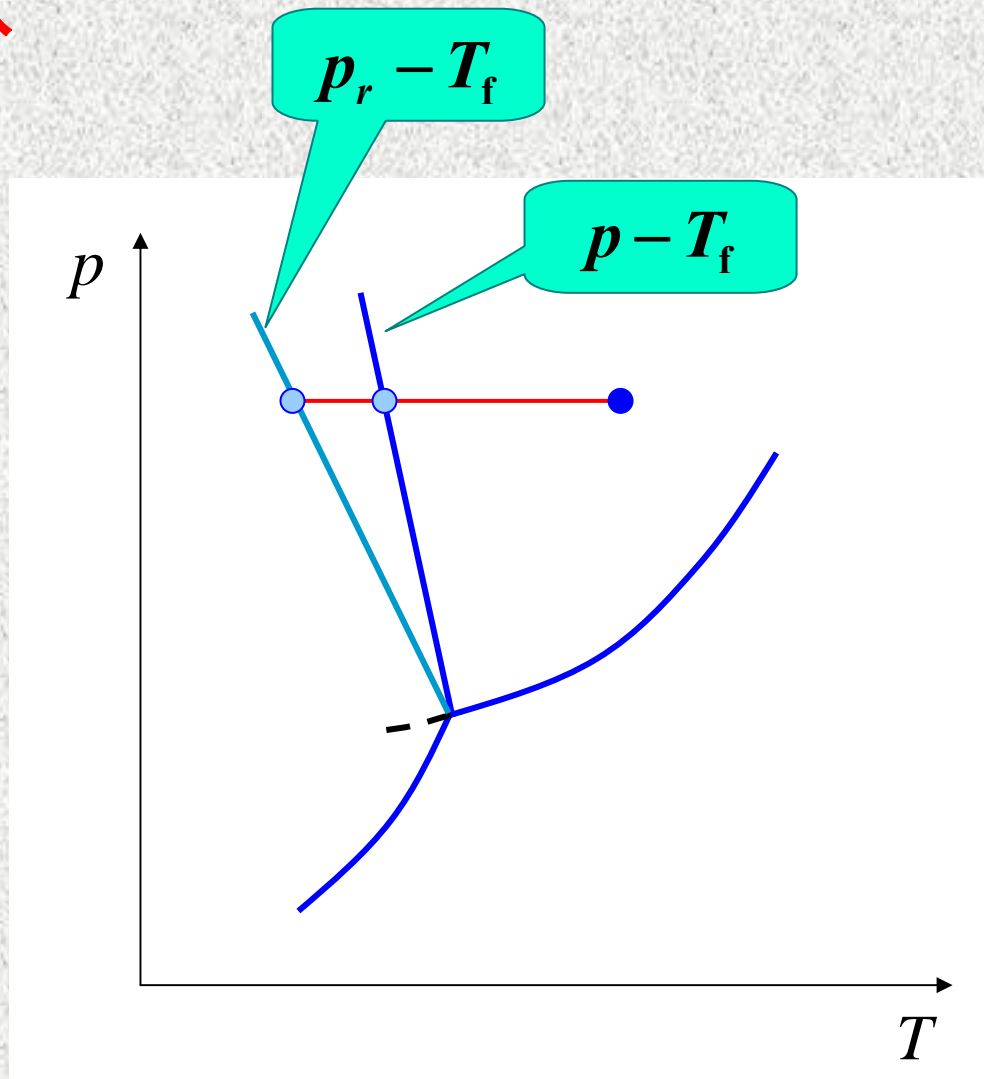
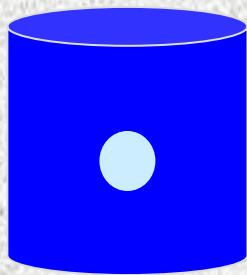


过热液体

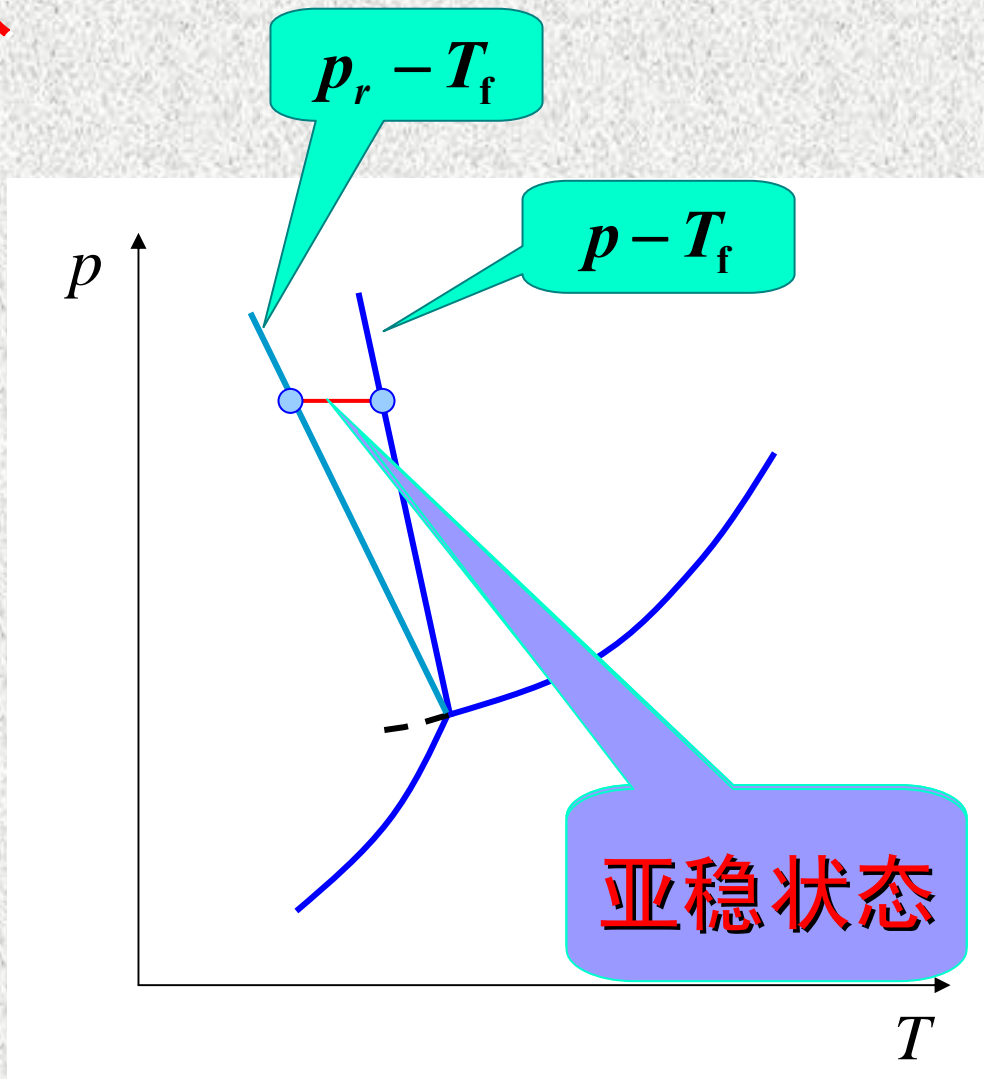
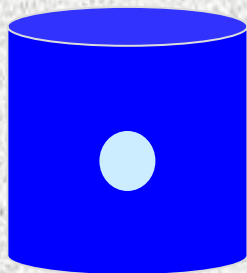


亚稳状态

过冷液体



过冷液体



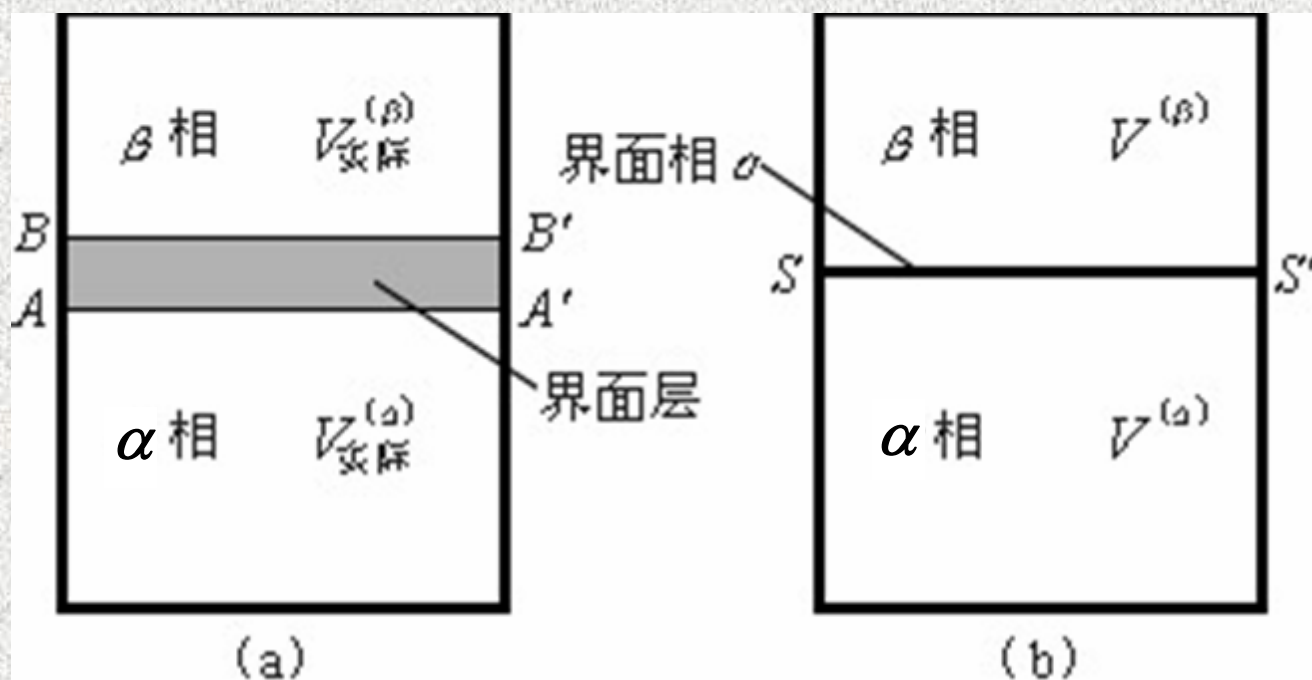
15-6

吉布斯等温方程

物理化学多媒体课堂教学软件 V1.0版

吉布斯界面模型

- ◆ 将界面层抽象为无厚度无体积的平面界面相，以符号 σ 表示
- ◆ 相和相的强度性质与实际系统中 α 相和 β 相的强度性质完全相同



界面过剩量和单位界面过剩量

$$\begin{aligned}n_i^{(\sigma)} &\stackrel{\text{def}}{=} n_i - n_i^{(\alpha)} - n_i^{(\beta)} \\ &= n_i - V^{(\alpha)} c_i^{(\alpha)} - V^{(\beta)} c_i^{(\beta)}\end{aligned}$$

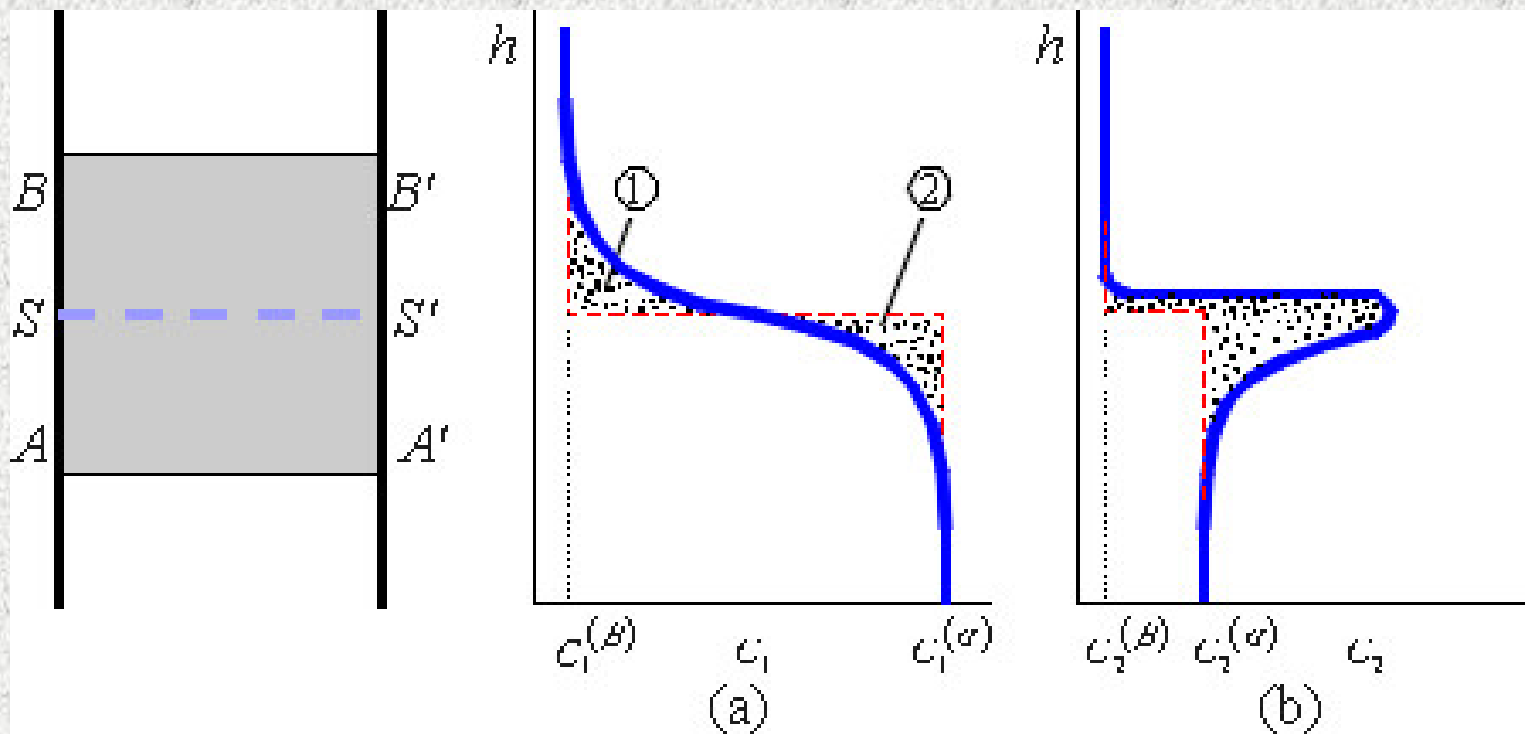
$$n_i^{(\sigma)} > 0 \quad \text{正吸附}$$

$$n_i^{(\sigma)} < 0 \quad \text{负吸附}$$

$$\Gamma_i \stackrel{\text{def}}{=} n_i^{(\sigma)} / A_s$$

吉布斯单位界面过剩量

$$\Gamma_i^{(1)} \stackrel{\text{def}}{=} \Gamma_i \quad (\Gamma_1 = 0) \quad \Gamma_1^{(1)} = 0$$



1. 吉布斯等温方程的推导

根据界面相的G-D方程

$$0 = S^{(\sigma)} dT^{(\sigma)} + A_s d\sigma + \sum_i n_i^{(\sigma)} d\mu_i^{(\sigma)}$$

$$\left(\right)_T \quad 0 = A_s d\sigma + \sum_i n_i^{(\sigma)} d\mu_i^{(\sigma)}$$

定义 $\Gamma_i = n_i^{(\sigma)} / A_s$ 单位界面过剩量

吉布斯模型 $\Gamma_i^{(1)} \quad \Gamma_1^{(1)} = 0$

$$-d\sigma = \sum_{i \neq 1} \Gamma_i^{(1)} d\mu_i \quad \text{——吉布斯等温方程}$$

1. 吉布斯等温方程的推导

根据界面相的G-D方程

$$0 = S^{(\sigma)} dT^{(\sigma)} + A_s d\sigma + \sum_i n_i^{(\sigma)} d\mu_i^{(\sigma)}$$

$$\left(\right)_T \quad 0 = d\sigma + \sum_i \Gamma_i d\mu_i^{(\sigma)}$$

定义 $\Gamma_i = n_i^{(\sigma)} / A_s$ 单位界面过剩量

吉布斯模型 $\Gamma_i^{(1)} \quad \Gamma_1^{(1)} = 0$

$$-d\sigma = \sum_{i \neq 1} \Gamma_i^{(1)} d\mu_i \quad \text{——吉布斯等温方程}$$

$$-d\sigma = \sum_{i \neq 1} \Gamma_i^{(1)} d\mu_i$$

二元系

$$-d\sigma = \Gamma_2^{(1)} d\mu_2$$

$$\Gamma_2^{(1)} = - \left(\frac{\partial \sigma}{\partial \mu_2} \right)_T$$

——吉布斯等温方程

$$\mu_2 = \mu_{c,2}^{**} + RT \ln a_{c,2}$$

$$d\mu_2 = RT d \ln a_{c,2}$$

$$\Gamma_2^{(1)} = -\frac{1}{RT} \left(\frac{\partial \sigma}{\partial \ln a_{c,2}} \right)_T = -\frac{a_{c,2}}{RT} \left(\frac{\partial \sigma}{\partial a_{c,2}} \right)_T$$

稀溶液

$$\Gamma_2^{(1)} \approx -\frac{c_2}{RT} \left(\frac{\partial \sigma}{\partial c_2} \right)_T$$

2. 正吸附与负吸附

$$\Gamma_2^{(1)} \approx -\frac{c_2}{RT} \left(\frac{\partial \sigma}{\partial c_2} \right)_T$$

正吸附

$$\Gamma_2^{(1)} > 0$$

$$\left(\frac{\partial \sigma}{\partial c_2} \right)_T < 0$$

负吸附

$$\Gamma_2^{(1)} < 0$$

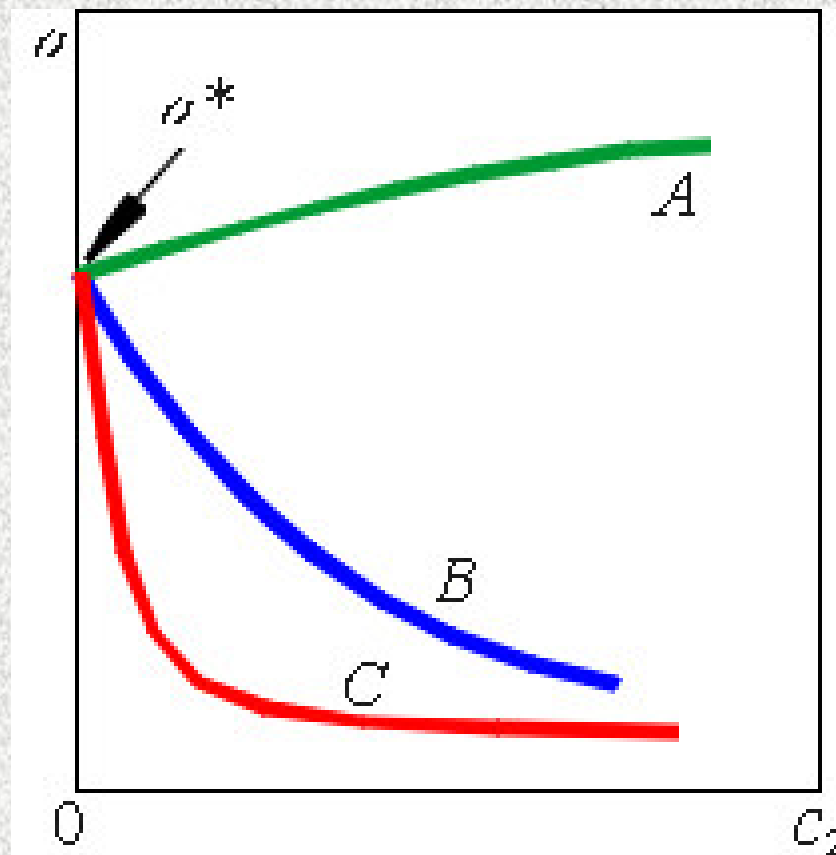
$$\left(\frac{\partial \sigma}{\partial c_2} \right)_T > 0$$

肥皂、8碳以上直链有机酸的碱金属盐、高碳直链烷基硫酸盐和苯磺酸盐等

--- 表面活性剂

醇、醛、酮、羧酸、酯等有机物

NaCl、 Na_2SO_4 、KOH、 NH_4Cl 、 KNO_3 等无机盐类，以及蔗糖、甘露醇等多羟基有机物



3. 表面活性物质

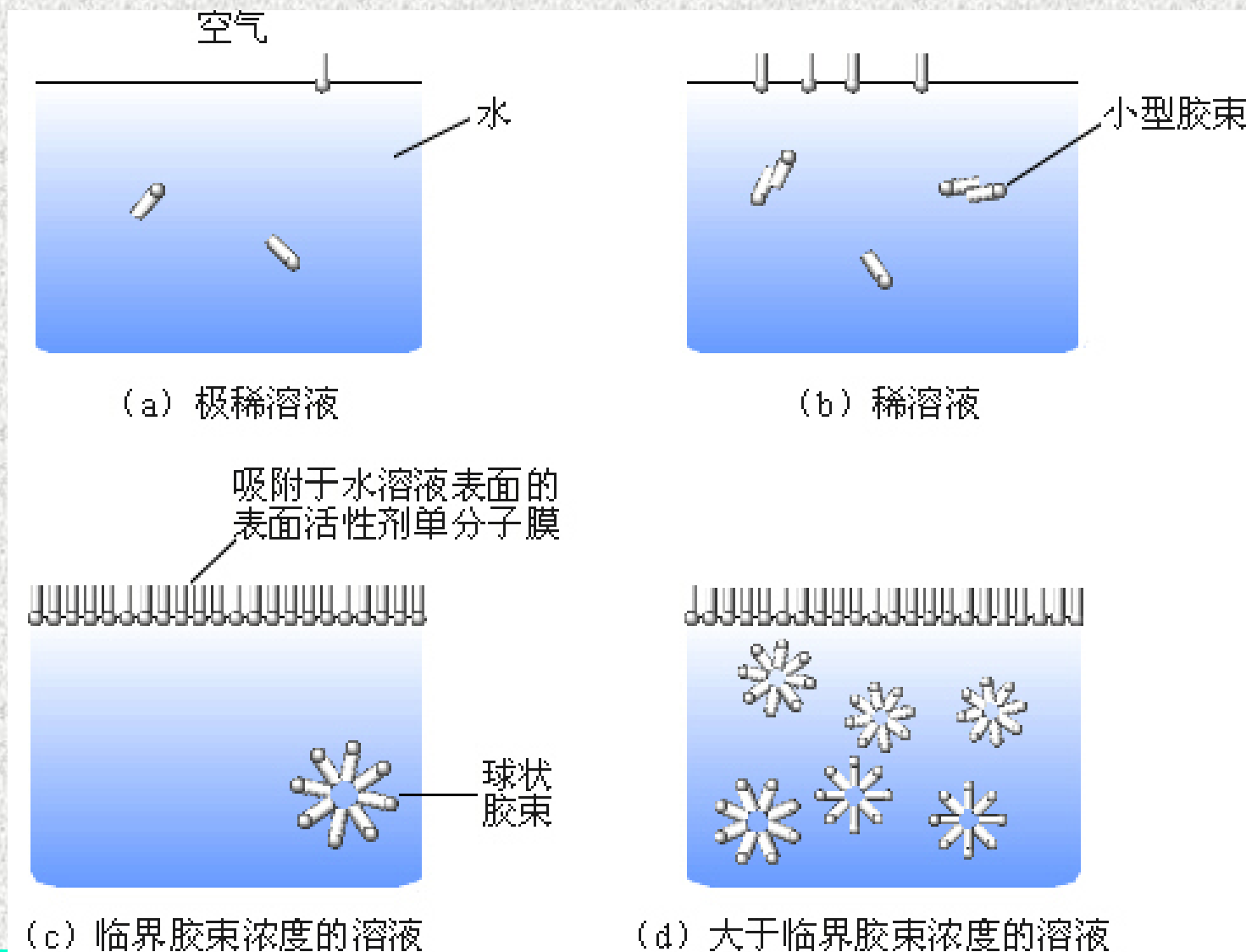
能显著降低水气界面和水油界面的界面张力的物质。称表面活性物质。又称表面活性剂



亲油基：含有8个碳原子以上的碳链。

亲水基：可以是带电基团；或两性离子；也可以极性基团。

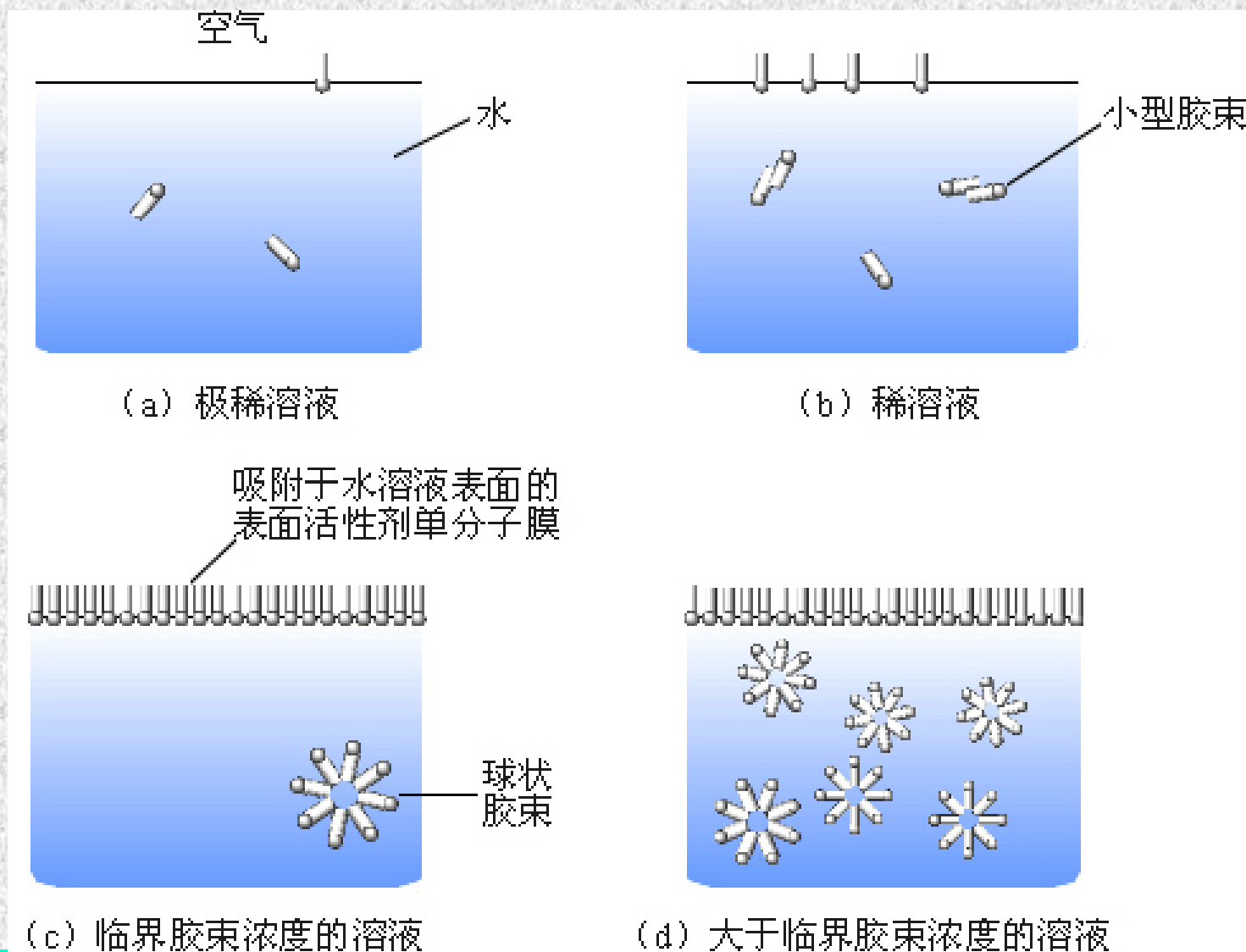
4. 胶束和临界胶束浓度



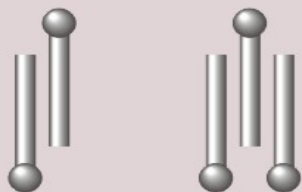
4. 胶束和临界胶束浓度

- ◆ 胶束 表面活性物质分子的聚集体。
- ◆ 临界胶束浓度 表面活性物质形成球形胶束的最低浓度。可用 cmc 表示

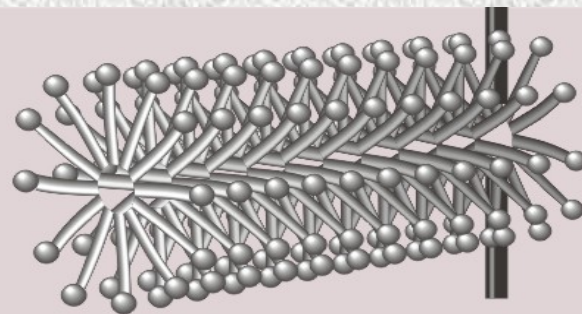
4. 胶束和临界胶束浓度



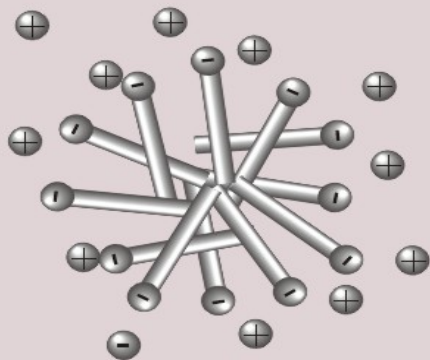
4. 胶束和临界胶束浓度



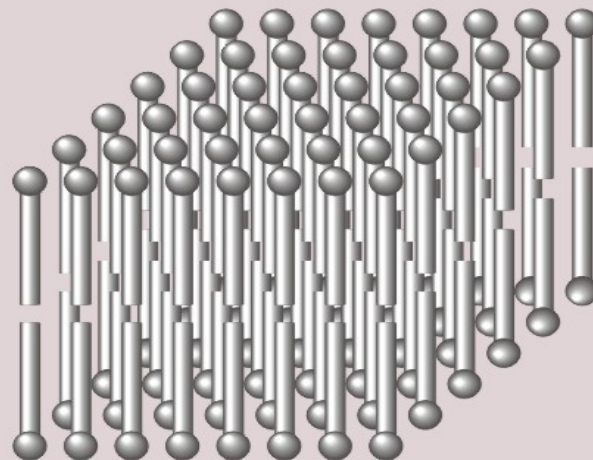
小型胶束



棒状胶束



球状胶束



层状胶束

4. 胶束和临界胶束浓度

- ◆ 胶束 表面活性物质分子的聚集体。
- ◆ 临界胶束浓度 表面活性物质形成球形胶束的最低浓度。可用 cmc 表示
- ◆ 增溶作用 当浓度超过 cmc 后，在溶液内部所生成的胶束，往往能使一些不易溶于水的物质因进入胶束而增加其溶解度。

5. 实验测定界面张力

毛细管上升下降法

$$\sigma = R\rho^{(l)}gh/(2\cos\theta)$$

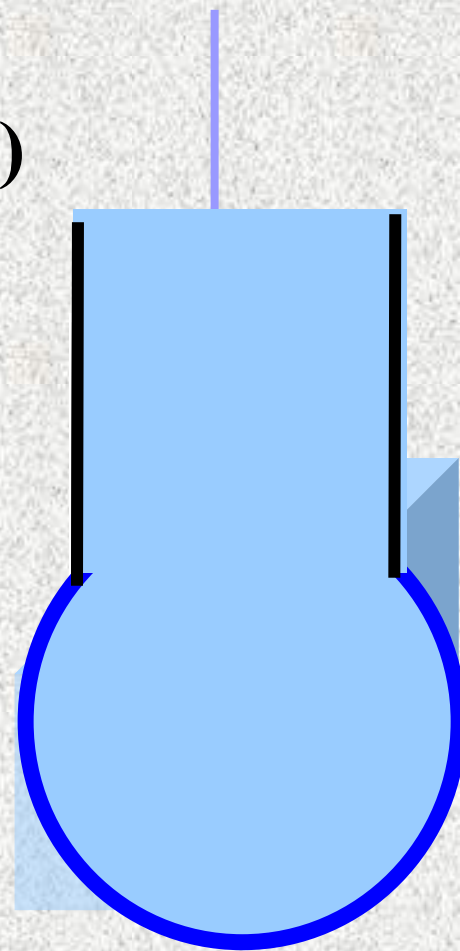
最大泡压法

$$\Delta p = 2\sigma / r$$

滴重法

$$mg = 2\pi r\sigma$$

吊板法,吊环法



6. 界面张力的半经验估算方法

稀溶液

$$\sigma^* - \sigma = bc_2$$

浓溶液

$$\sigma^* - \sigma = A + b \ln c_2$$

7. 界面张力的理论研究

$$A = -kT \ln Z$$

$$\sigma = \left(\frac{\partial A^{(\sigma)}}{\partial A_s} \right)_{T, V, n_j} = -kT \left(\frac{\partial \ln Z}{\partial A_s} \right)_{T, V, n_j}$$

15-7 润湿作用

物理化学多媒体课堂教学软件 V1.0版

将液体滴在固体表面上，由于性质不同，有的会铺展开来，有的则粘附在表面上成为平凸透镜状，这种现象称为**润湿作用**。

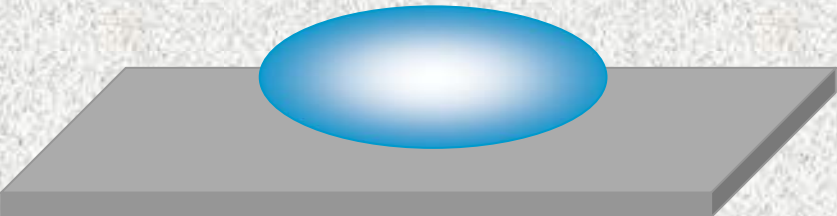




铺展润湿



粘附润湿



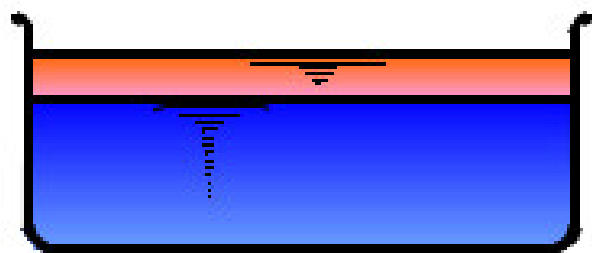
不润湿



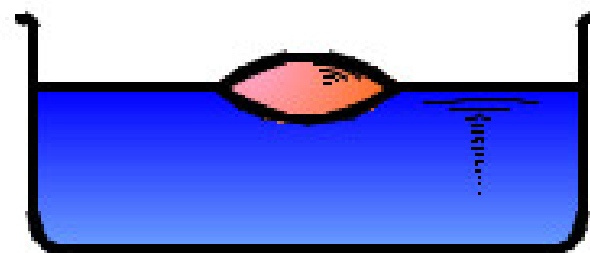
铺展润湿

粘附湿润

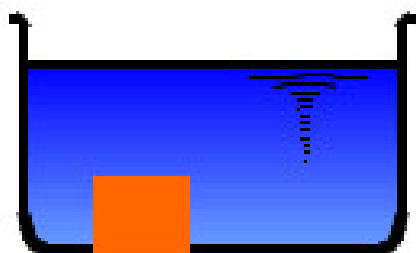
不湿润



铺展

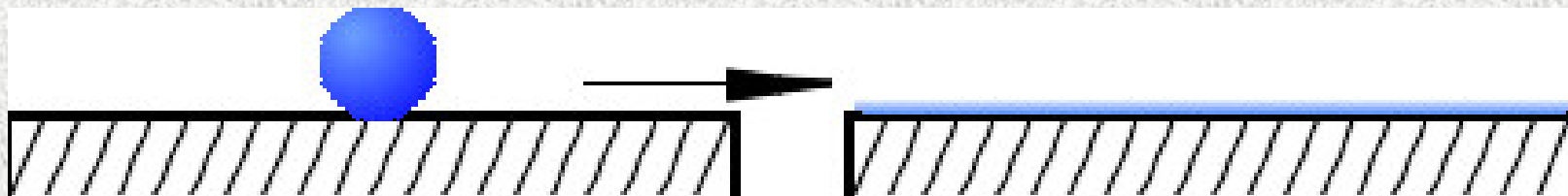


不铺展



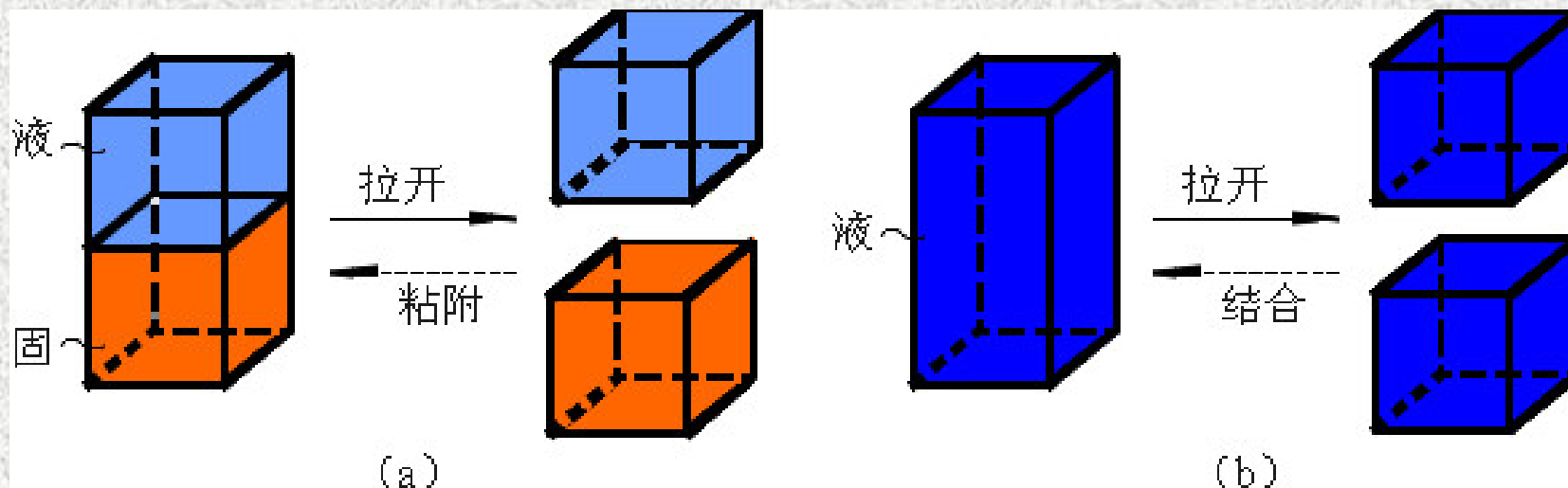
浸湿

1. 铺展系数 φ



$$\Delta G = A_s (\sigma_{\text{液,固}} + \sigma_{\text{气,液}} - \sigma_{\text{气,固}})$$

$$\varphi \stackrel{\text{def}}{=} -(\sigma_{\text{液,固}} + \sigma_{\text{气,液}} - \sigma_{\text{气,固}}) = -\Delta G / A_s$$



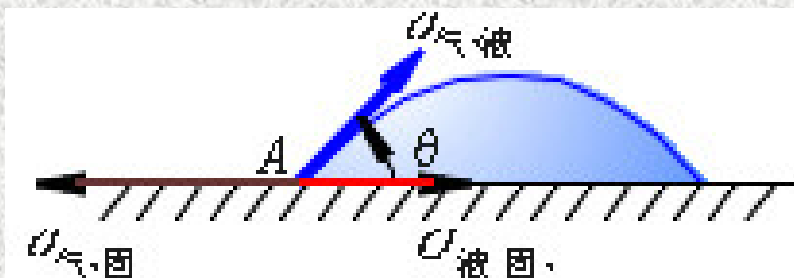
$$\varphi = (\sigma_{\text{气,液}} + \sigma_{\text{气,固}} - \sigma_{\text{液,固}}) - 2\sigma_{\text{气,液}}$$

$$W_a = \sigma_{\text{气,液}} + \sigma_{\text{气,固}} - \sigma_{\text{液,固}}$$

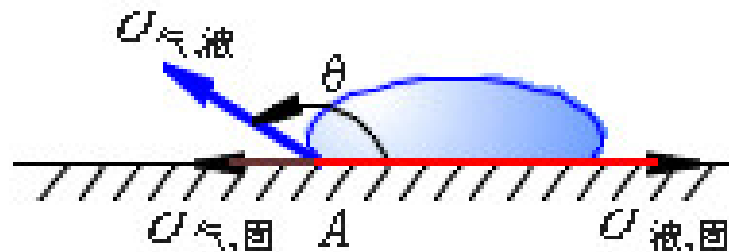
$$W_c = 2\sigma_{\text{气,液}}$$

$$\varphi = W_a - W_c$$

2. 接触角与杨氏方程



(a) 粘附润湿



(b) 不润湿

$$\cos \theta > 0$$

$$\theta < 90^\circ$$

粘附润湿

$$\sigma_{\text{气,固}} = \sigma_{\text{液,固}} + \sigma_{\text{气,液}} \cos \theta$$

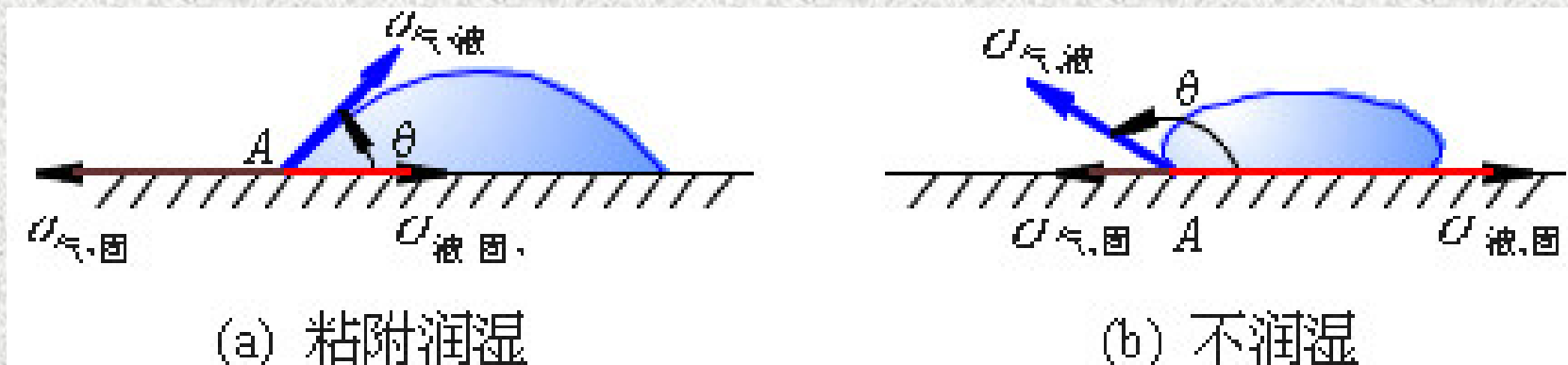
$$\cos \theta = \frac{\sigma_{\text{气,固}} - \sigma_{\text{液,固}}}{\sigma_{\text{气,液}}}$$

$$\cos \theta < 0$$

$$\theta > 90^\circ$$

不润湿

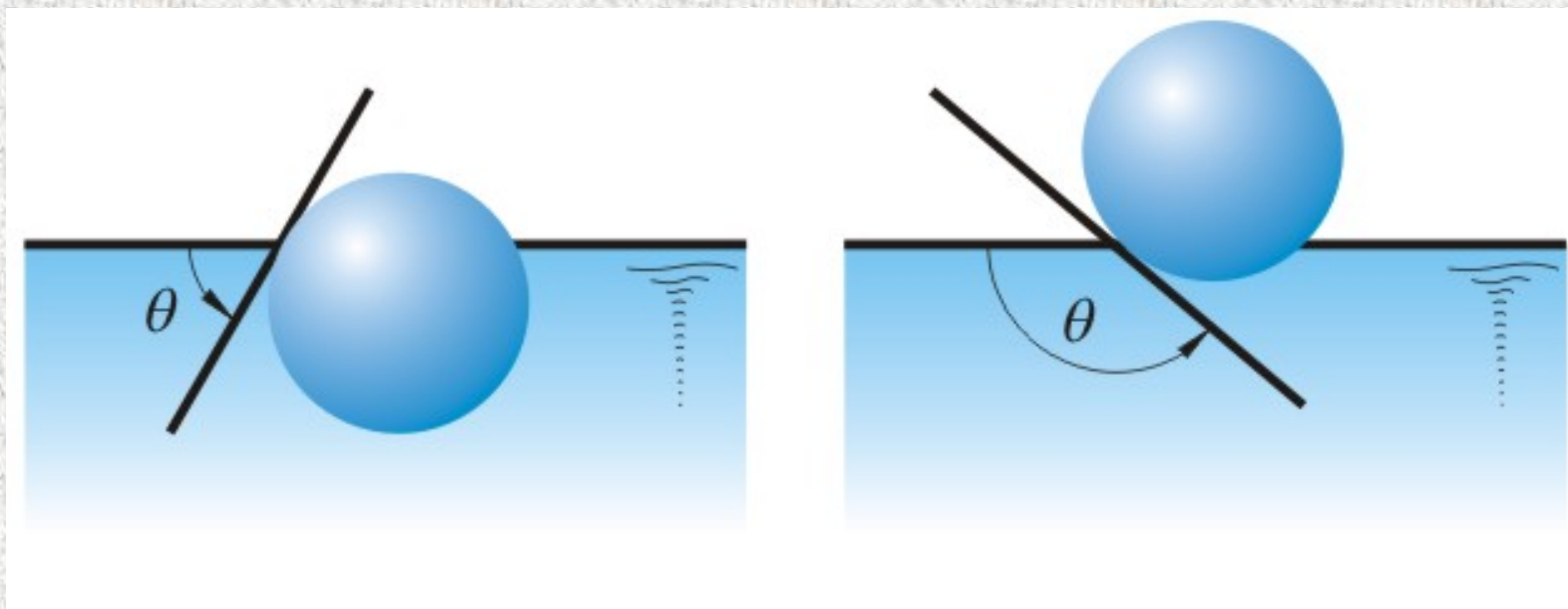
2. 接触角与杨氏方程



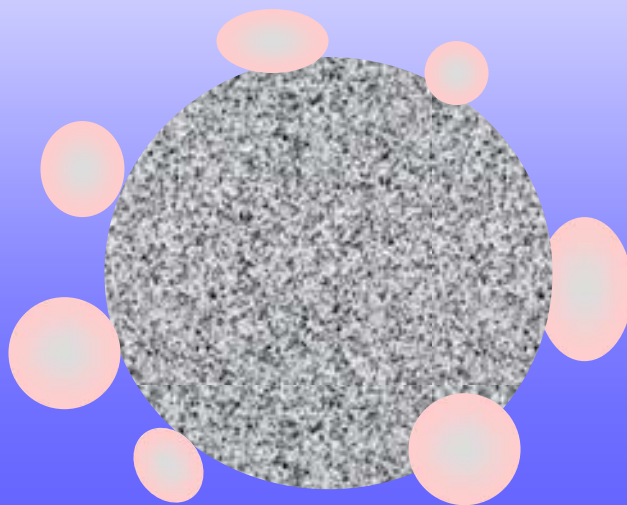
$$W_a = \sigma_{\text{气,液}} (1 + \cos \theta)$$

$$\varphi = \sigma_{\text{气,液}} (\cos \theta - 1)$$

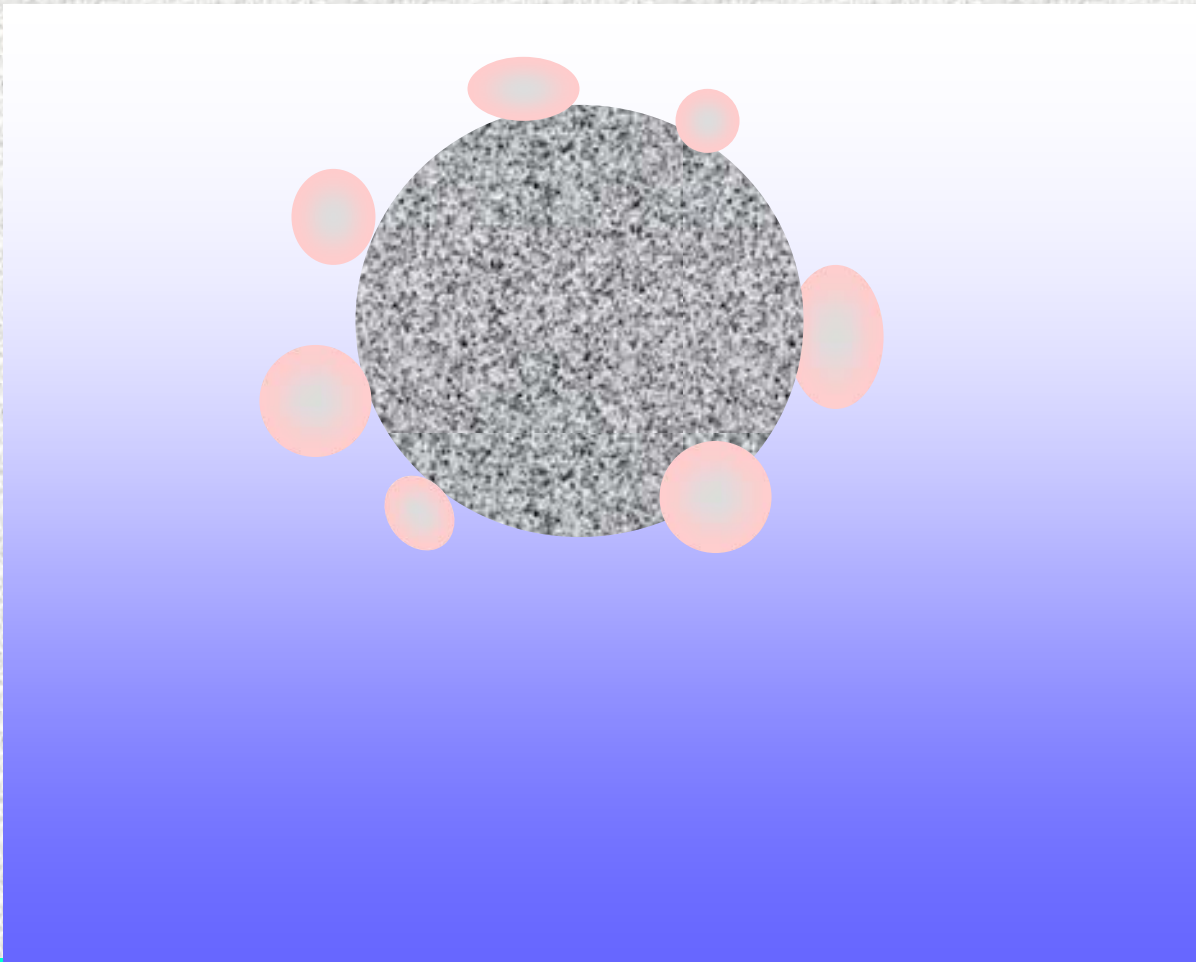
3. 表面活性物质与润湿作用



泡沫浮选法



泡沫浮选法



$\sigma_{g,w}$ 大, $\sigma_{g,0} + \sigma_{w,0}$ 小, $\varphi > 0$ 铺展

$\sigma_{g,w}$ 小, $\sigma_{g,0} + \sigma_{w,0}$ 大, $\varphi < 0$ 不铺展

$$\varphi \stackrel{\text{def}}{=} -(\sigma_{\text{液,固}} + \sigma_{\text{气,液}} - \sigma_{\text{气,固}}) = -\Delta G / A_s$$

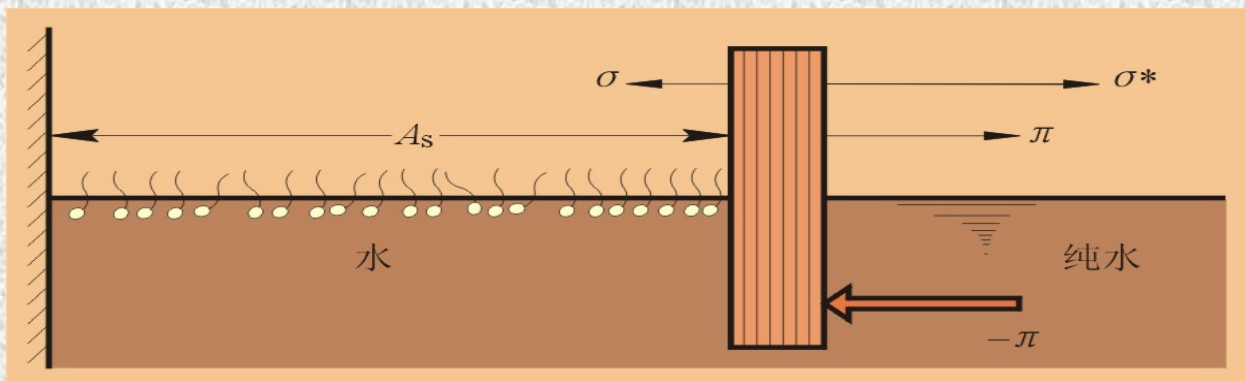
油中杂质使 $\sigma_{g,0}$ 减小, 有利于铺展

水中杂质使 $\sigma_{g,w}$ 减小, 不利于铺展

4. 不溶性单分子膜

——当表面活性物质在水中溶解度极小时，所形成的膜即为不溶性单分子膜。

❖ $\pi - A_s$ 关系 单分子膜可看作一种二维的流体。二维单分子膜在恒温下有一定 $\pi - A_s$ 的关系。

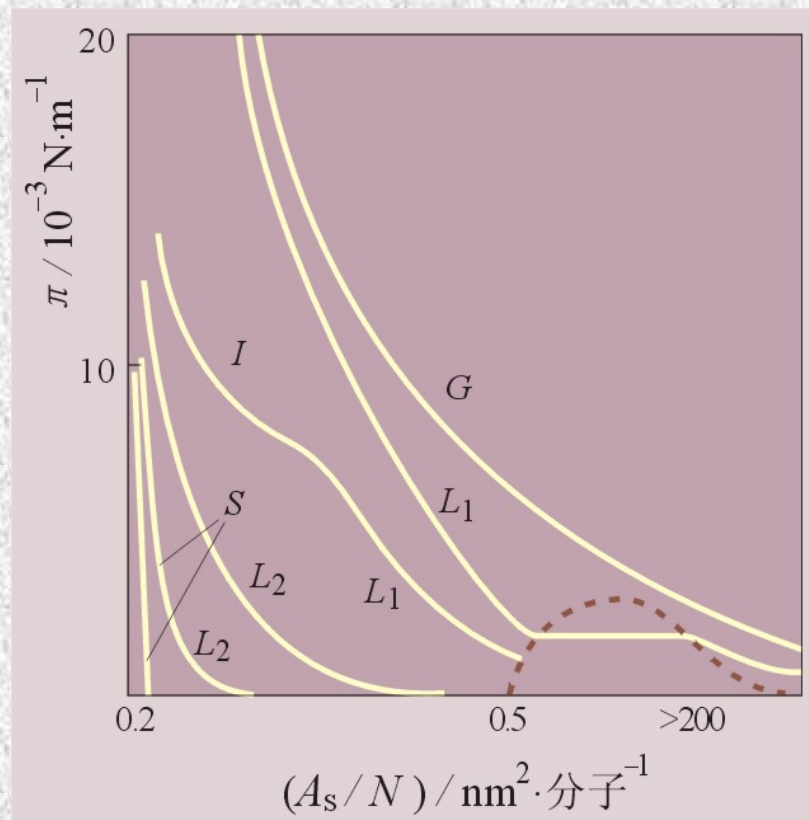


膜天平示意

4. 不溶性单分子膜

❖ $\pi - A_s$ 关系

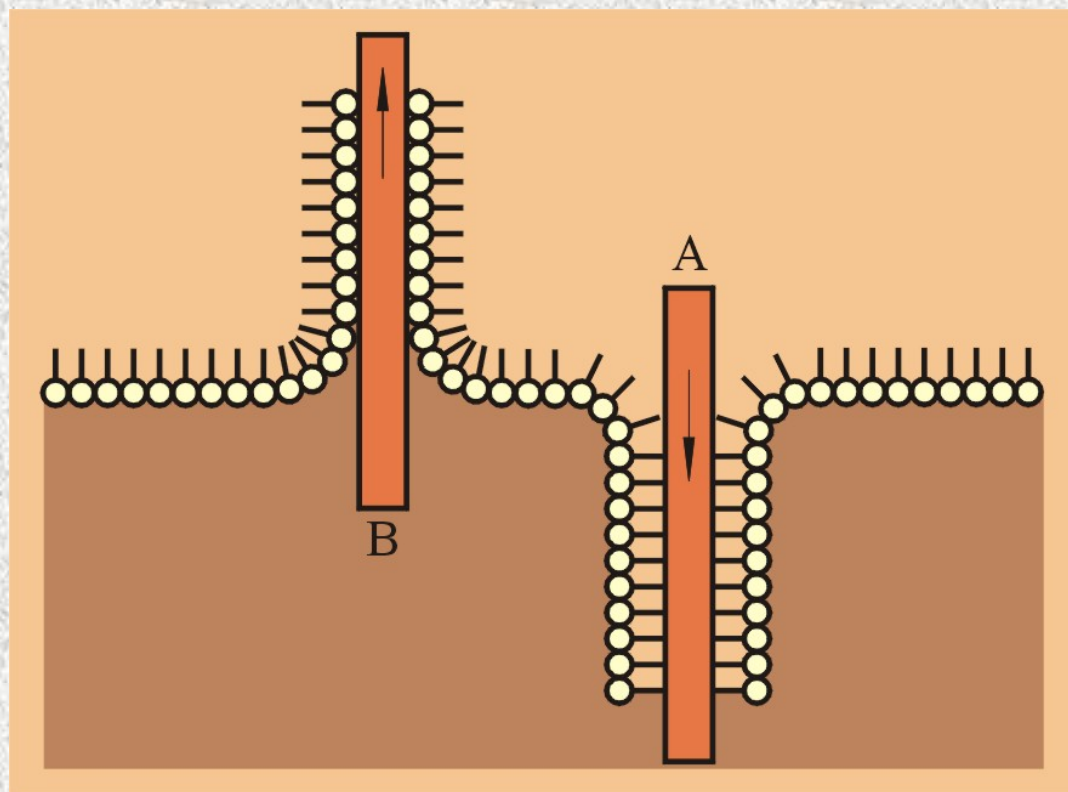
- 固态膜
- 凝聚液态膜
- 膨胀液态膜
- 气态膜



各种类型的 $\pi - A_s$ 关系

4. 不溶性单分子膜

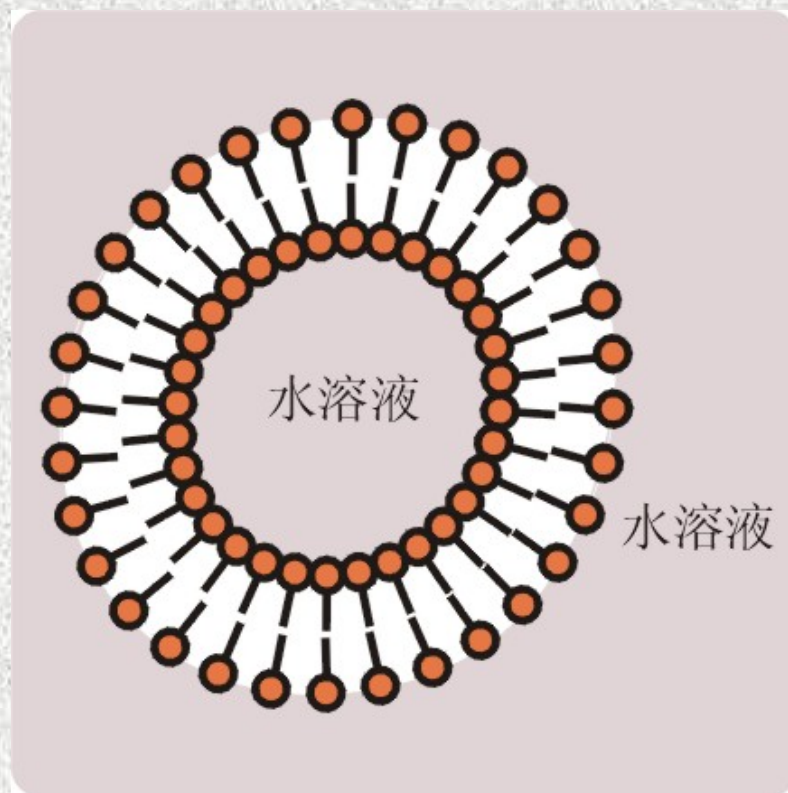
❖ LB膜



LB膜的制备

4. 不溶性单分子膜

❖ 双层膜和囊泡



囊泡

15-10 固体表面上的 的吸附作用

物理化学多媒体课堂教学软件 V1.0版

热力学第一、二定律

界面现象

考虑界面影响的热力学基本方程

对蒸汽压
的影响

吸 附

润湿与
铺展

$$f(T, \sigma, \Gamma, c) = 0$$

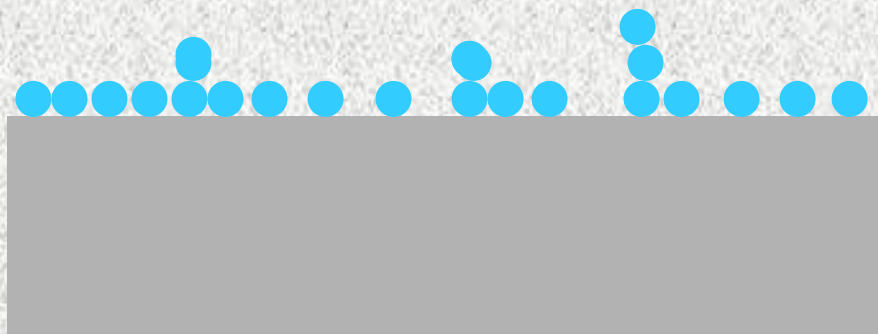
吸附模型

吸附平衡计算

1. 吸附与吸附量

吸附剂——具有吸附作用的固体物质；

吸附质——被吸附物质。



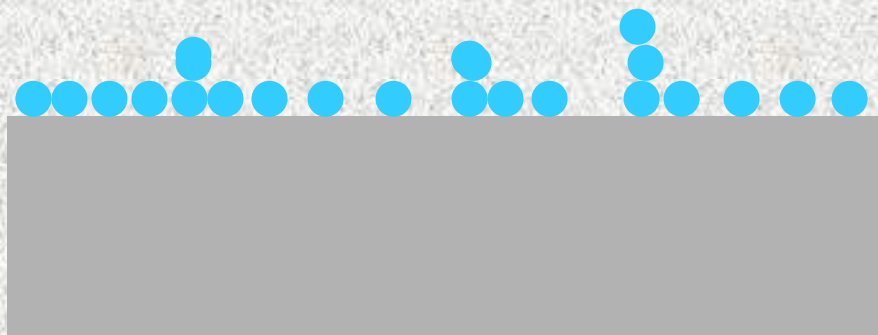
$$\Gamma_i = n_i^{(\sigma)} / A_s$$

$$\Gamma_i = V(i, \text{STP}) / A_s$$

$$\Gamma_i = n_i^{(\sigma)} / m$$

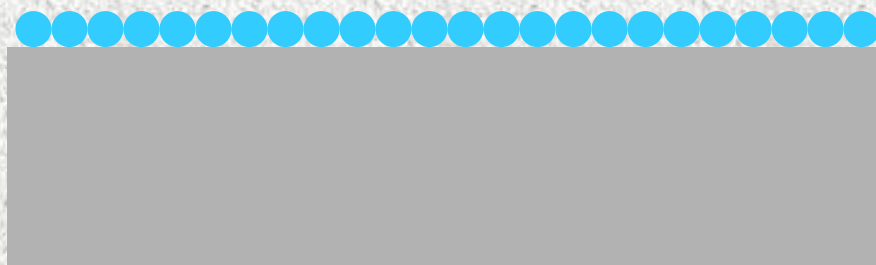
$$\Gamma_i = V(i, \text{STP}) / m$$

1. 吸附与吸附量



$$\theta \stackrel{\text{def}}{=} \Gamma / \Gamma_{\infty}$$

The equation defines the surface coverage θ as the ratio of the current surface concentration Γ to the maximum possible surface concentration Γ_{∞} . A red arrow points from the Γ term to the diagram above, and another red arrow points from the Γ_{∞} term to the diagram below.



2. 物理吸附与化学吸附

	物理吸附	化学吸附
机理:	范德华力	化学键, 表面化学反应
吸附层:	单分子或多分子层	单分子层
吸附热:	≈ 凝聚热	反应热
选择性:	无选择性	有选择性
可逆性:	可逆	多不可逆
速率:	较快, 易达平衡	较慢, 低温不易平衡

2. 物理吸附与化学吸附

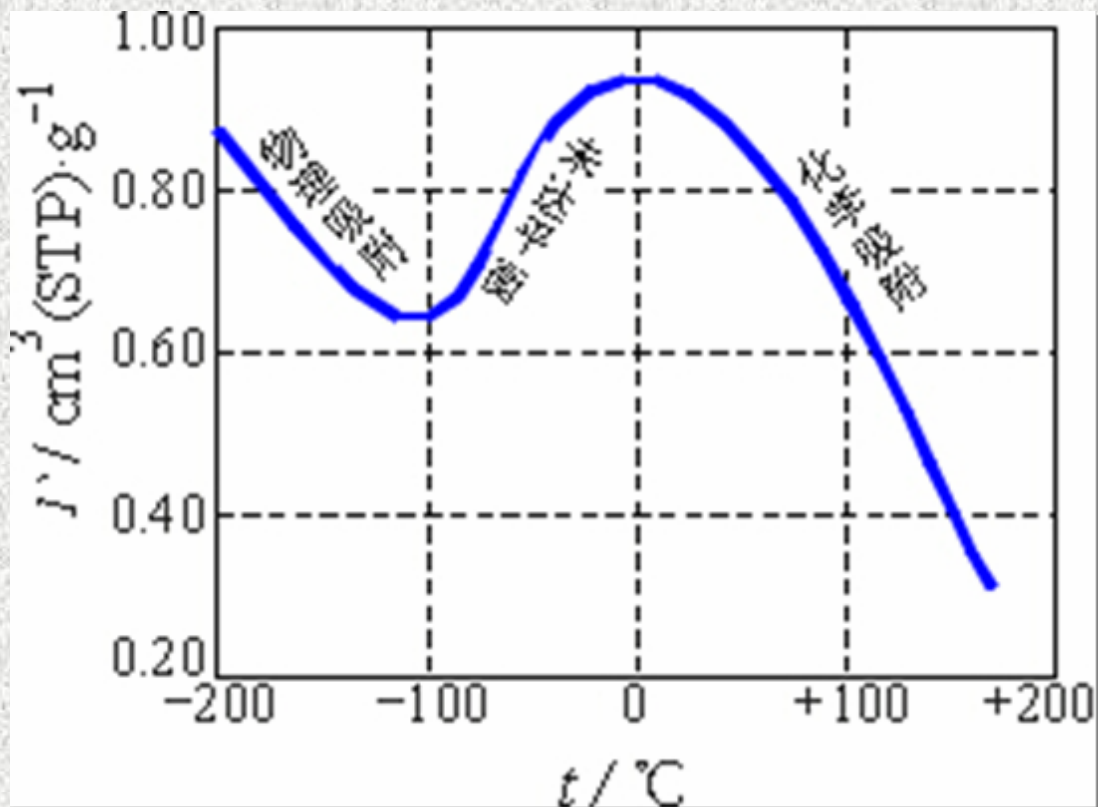
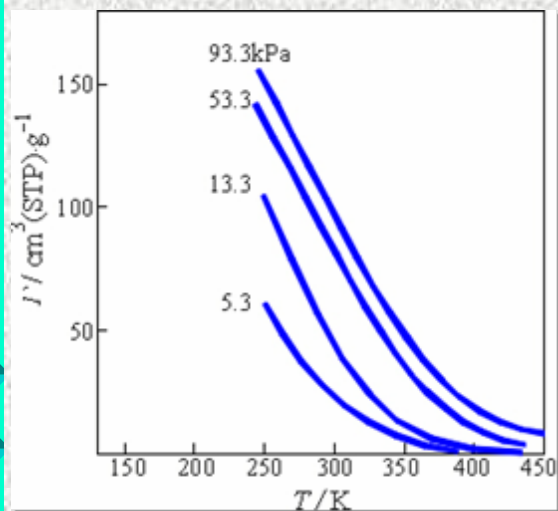
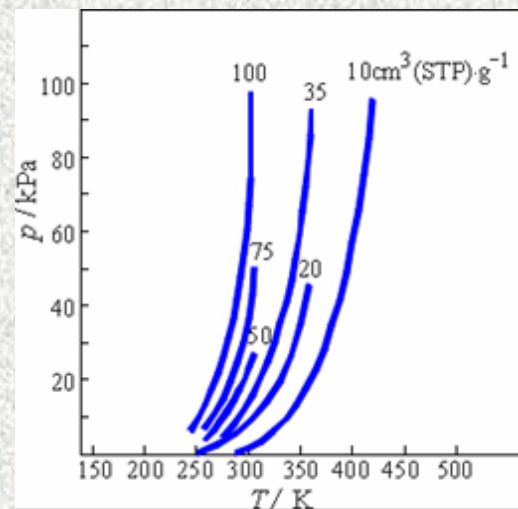


图15-39 CO在铂上的吸附等压线

3. 吸附量随温度、压力和体相浓度的变化



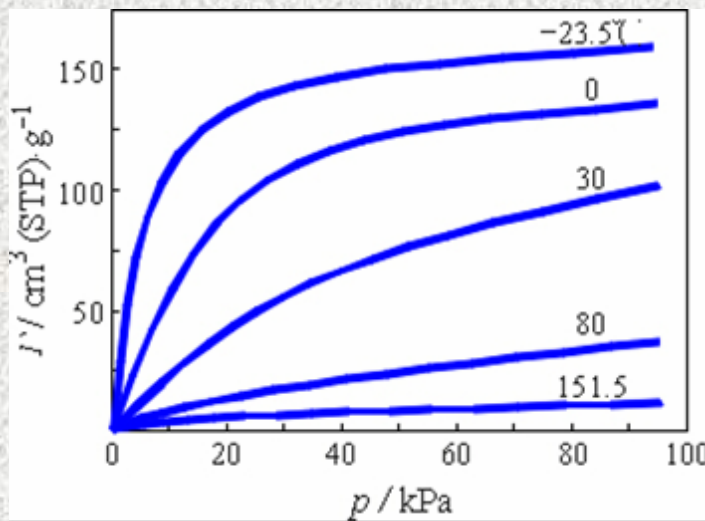
$$\Gamma = \Gamma(T, p)$$



$$\Gamma - p$$



$$\Gamma - T$$



$$T - p$$



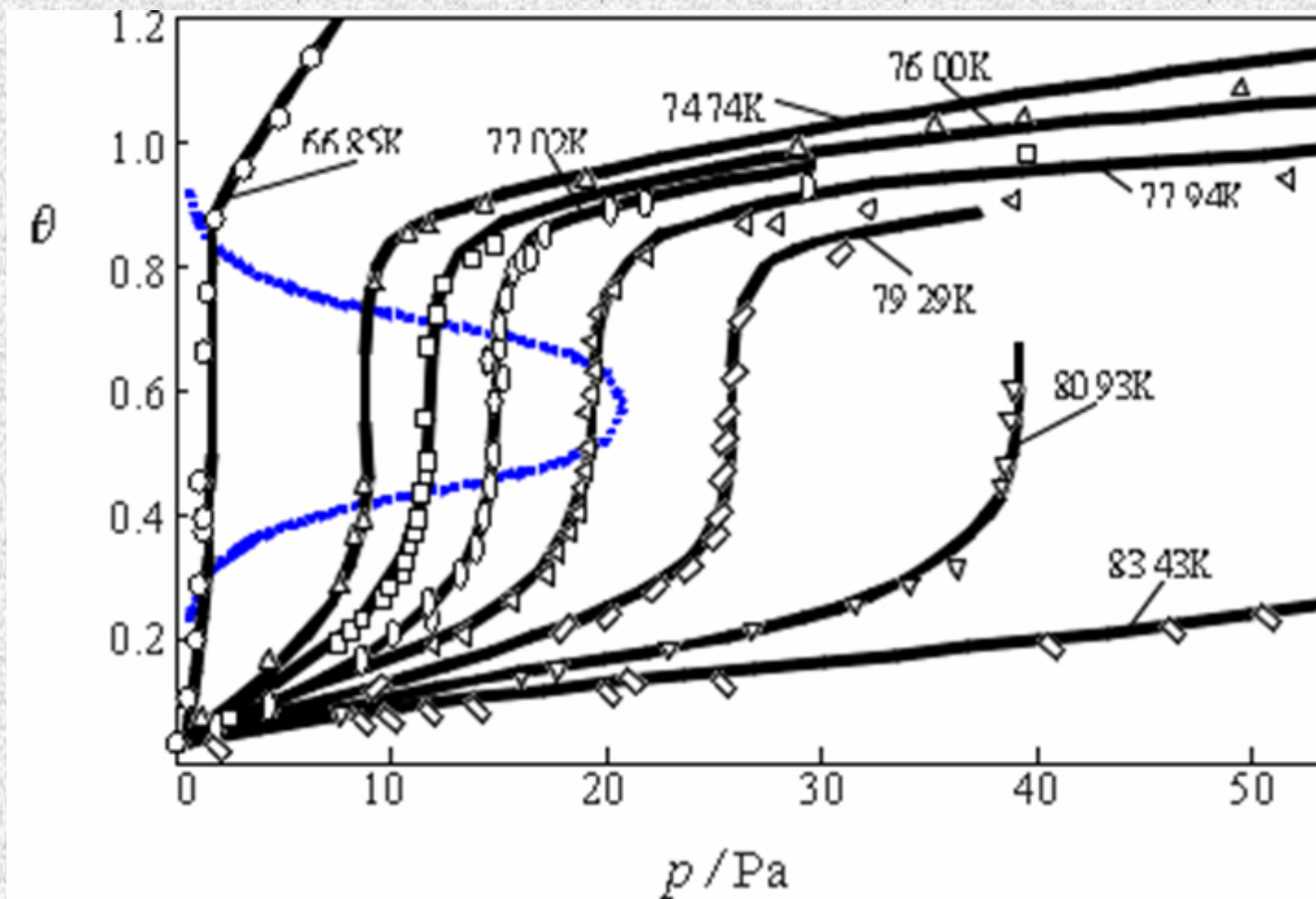
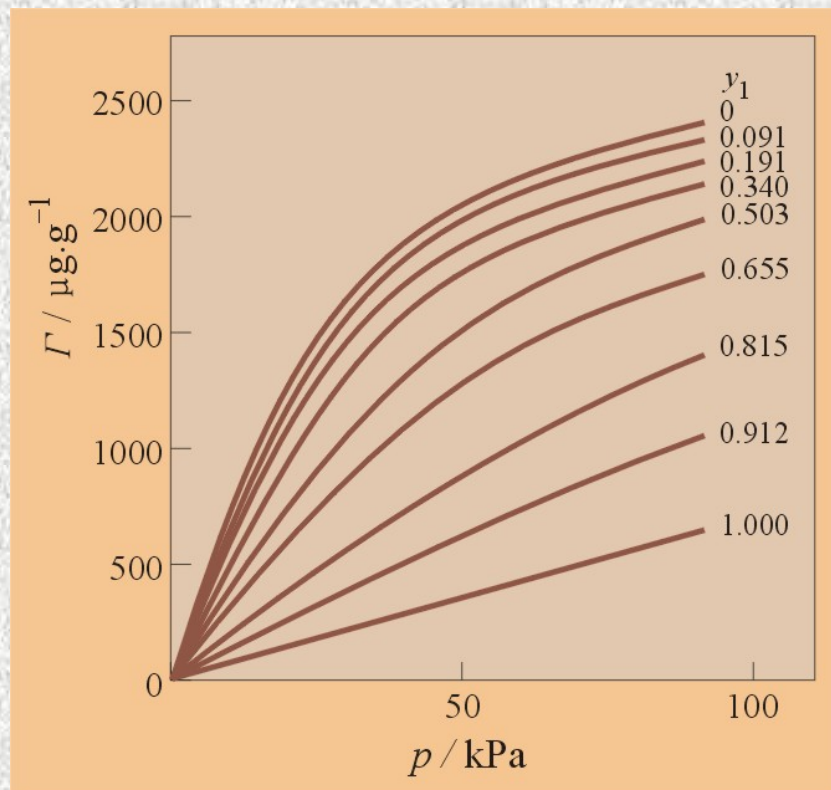


图15-34 Kr在NaBr上的吸附等温线

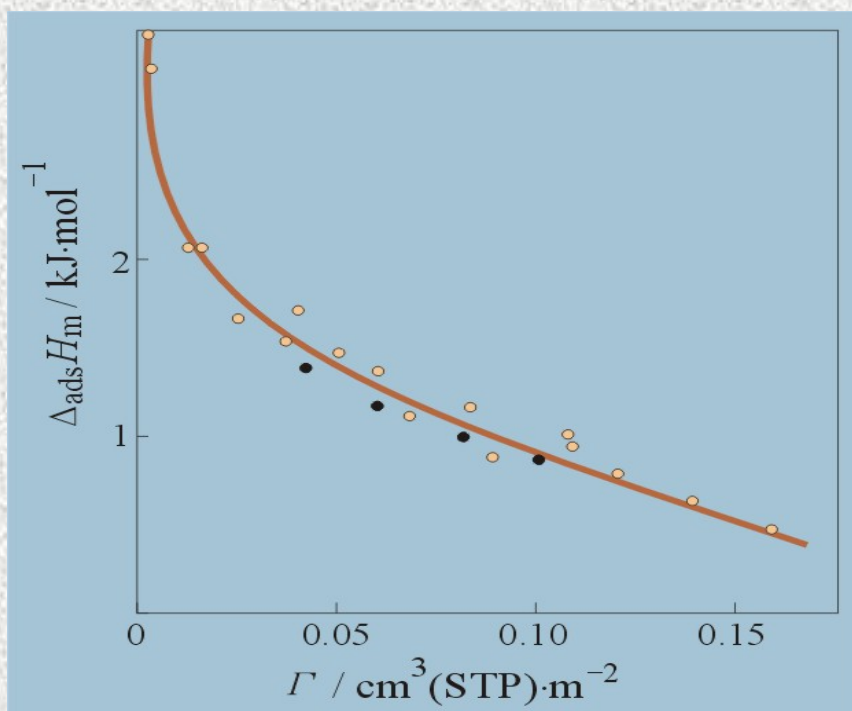
混合物的吸附等温线



25°C 下乙烷(1)-丙烷(2)
混合物在炭黑上的吸附等温线

吸附热

吸附热的绝对值随吸附量增大而减小，在吸附开始时减小尤为显著，这是由于表面非均一性而引起的。活性较高的部位优先吸附，吸附热也高。



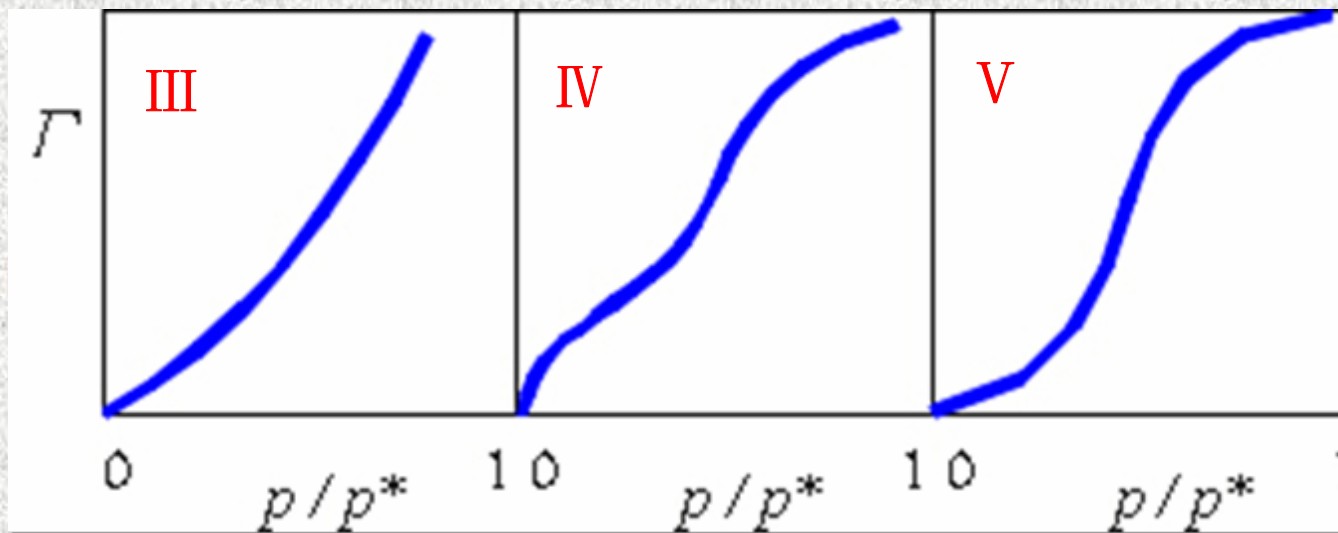
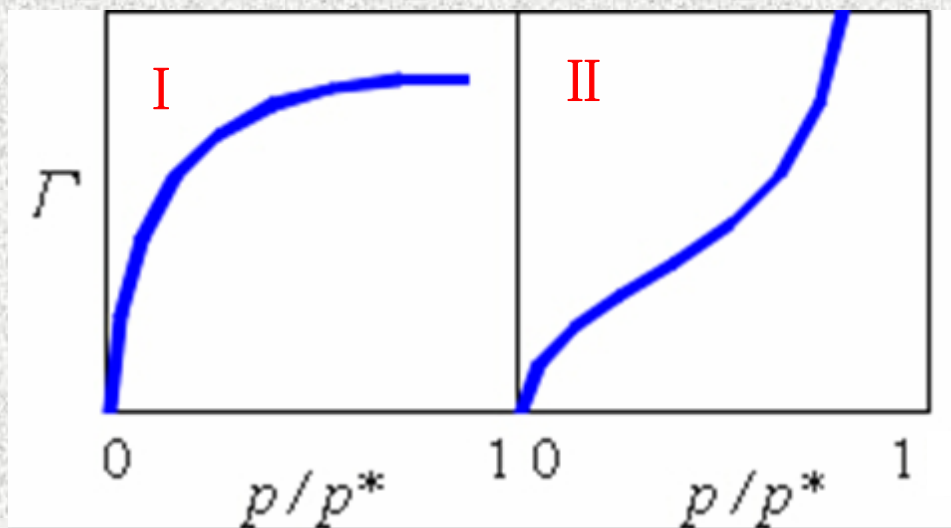
$$\Delta G < 0 \quad \Delta S < 0$$

$$\Delta G = \Delta H - T\Delta S$$

$$\Delta H < 0$$

吸附作用通常是放热的

吸附等温线的类型

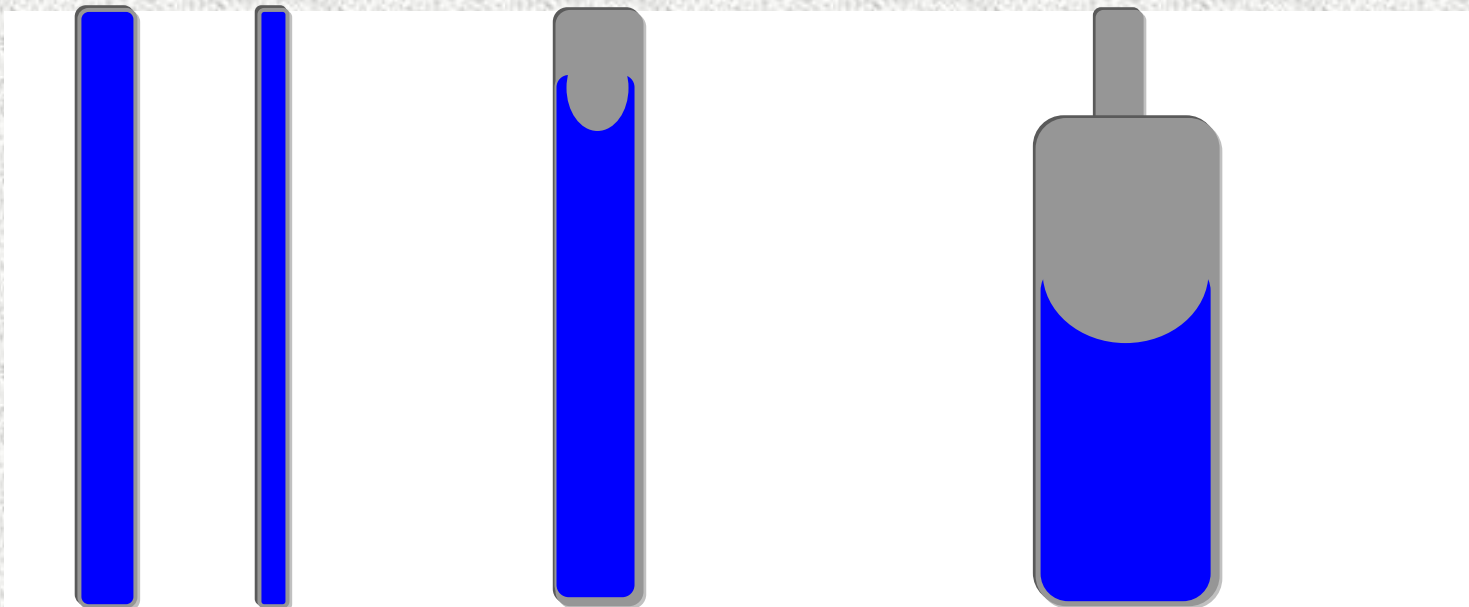


4. 毛细管凝结现象

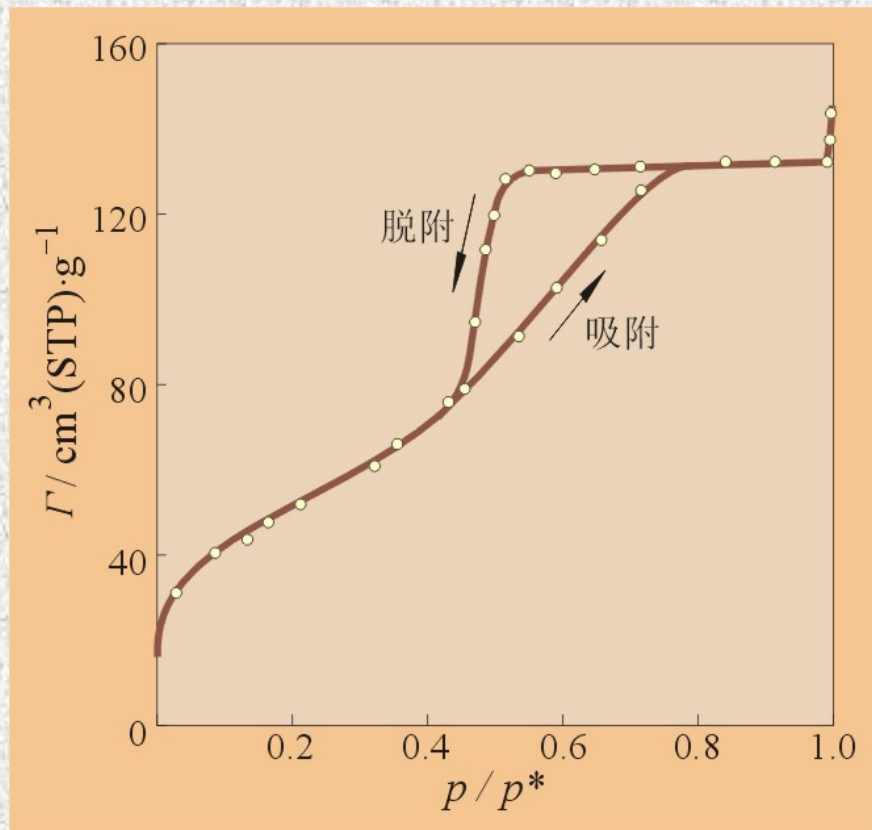
$$\ln \frac{p_r^*}{p^*} = - \frac{2\sigma M}{RT\rho r}$$

假设 $\theta = 0^\circ$

当 $p = p_r^*$

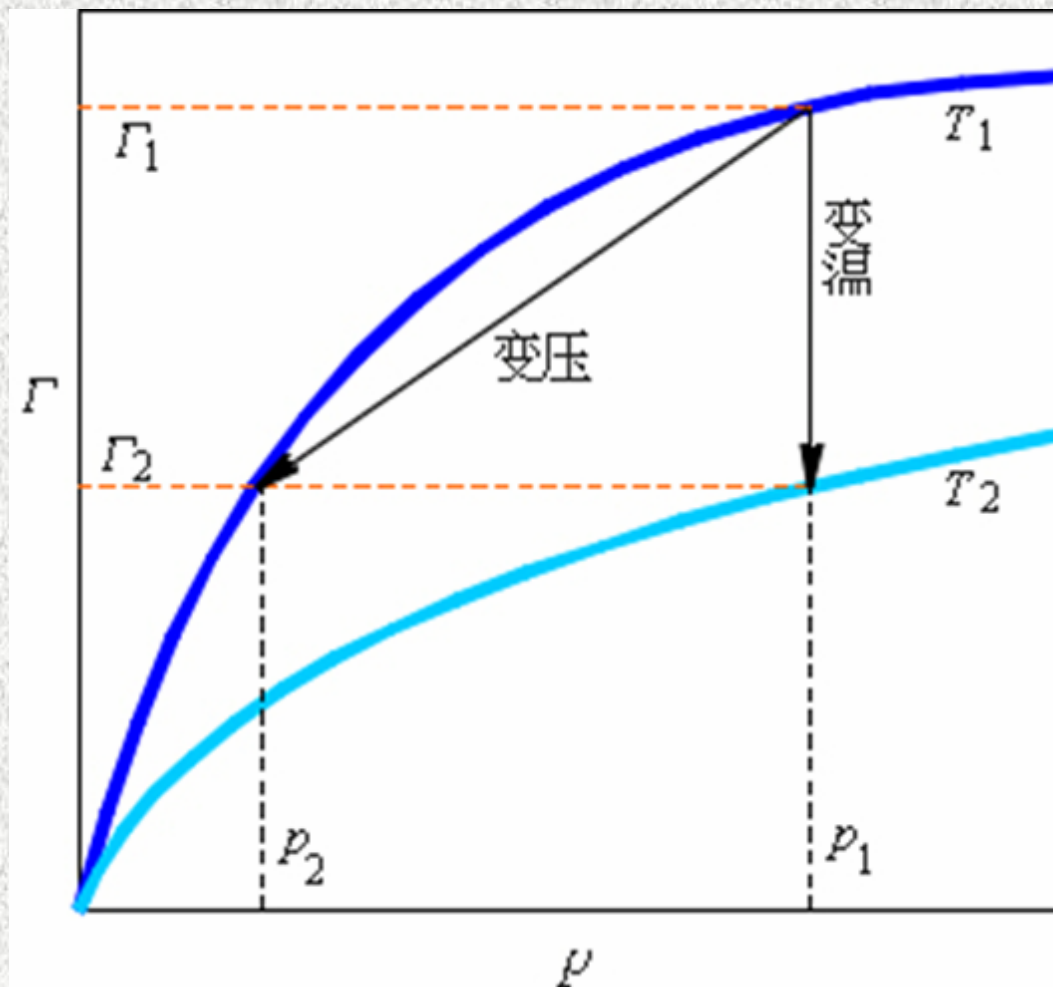


5. 脱附迟滞现象



N_2 在硅铝裂化催化剂上的
吸附与脱附

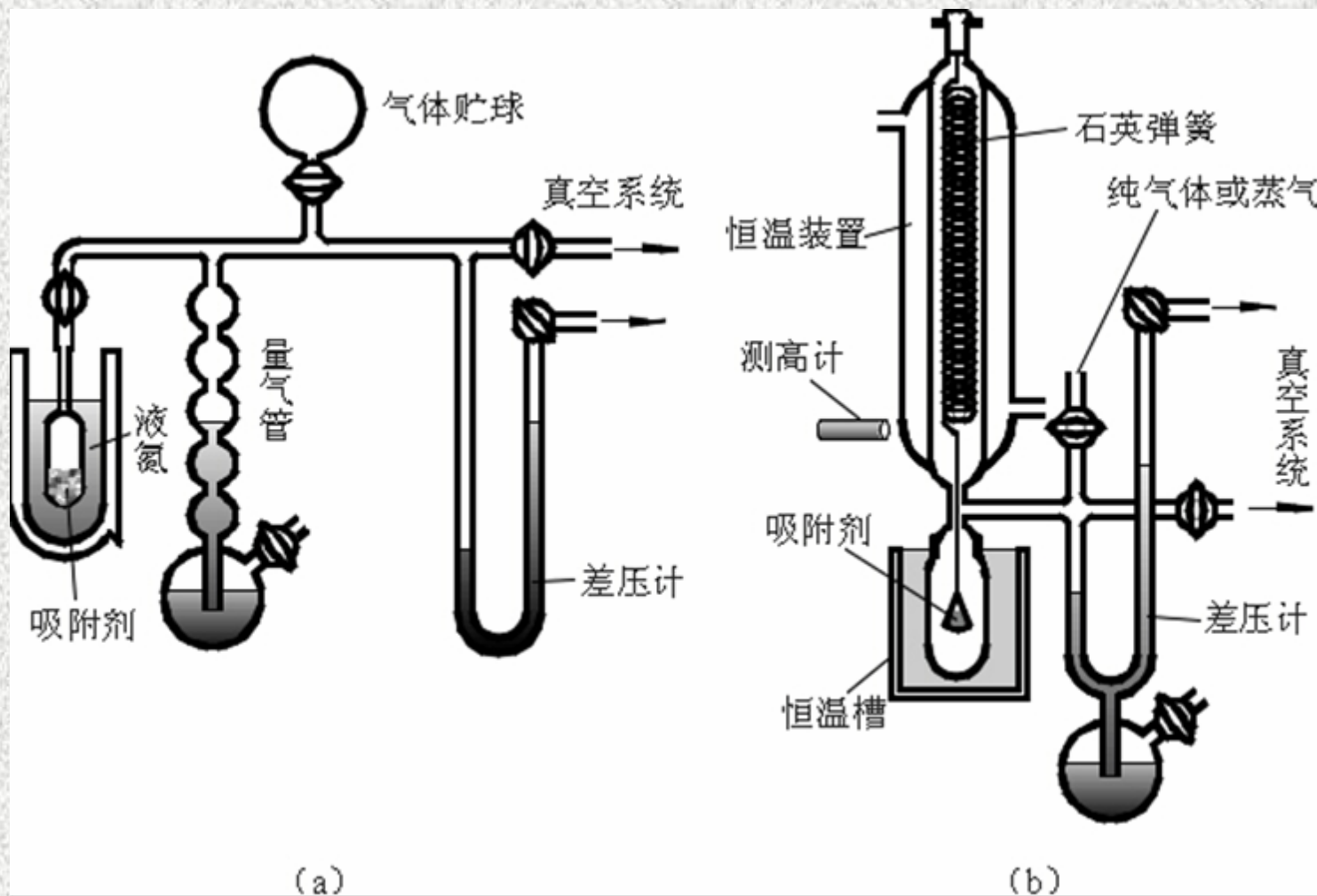
6. 变温吸附和变压吸附



15-11 固体吸附的实验、半经验 和理论方法

物理化学多媒体课堂教学软件 V1.0版

1. 实验方法



(a)

(b)

2. 半经验模型

(1) 弗罗因德利希(H.Freundlich)经验式

$$\Gamma = kp^{1/l}$$

$$\lg\{\Gamma\} = \lg\{k\} + l^{-1}\lg\{p\}$$

(2) 兰缪尔吸附等温式

适用于单分子层化学吸附

$$\Gamma = \Gamma_{\infty} \frac{bp}{1+bp}$$

$$\frac{p}{\Gamma} = \frac{1}{\Gamma_{\infty}b} + \frac{p}{\Gamma_{\infty}}$$

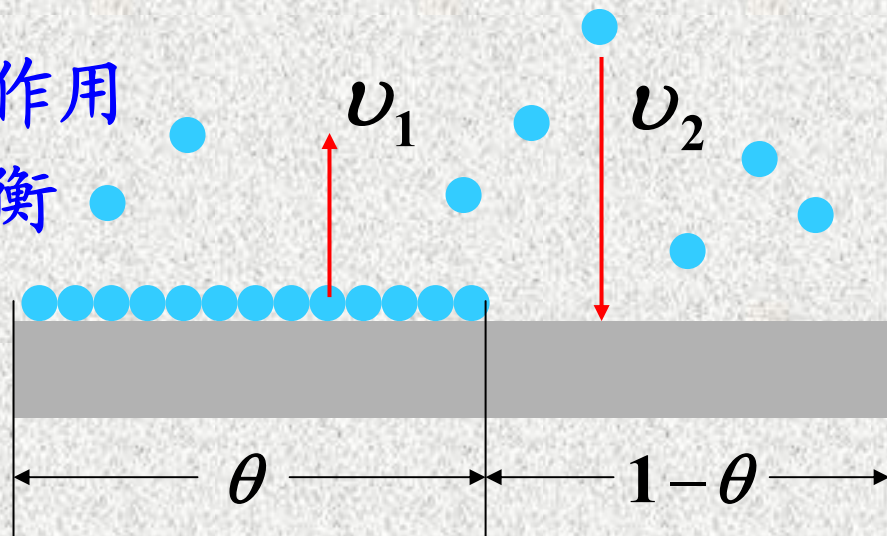
兰缪尔吸附模型

固体表面上各个原子的力场不饱和，可吸附碰撞到固体表面的气体分子或溶质分子

吸附理论的基本假设：

- ◆ 单分子层吸附
- ◆ 固体表面是均匀
- ◆ 吸附分子间无相互作用
- ◆ 吸附和脱附动态平衡

$$\theta = \frac{\Gamma}{\Gamma_{\infty}}$$



$$v_1 = k_1 \theta \quad v_2 = k_2 p(1 - \theta)$$

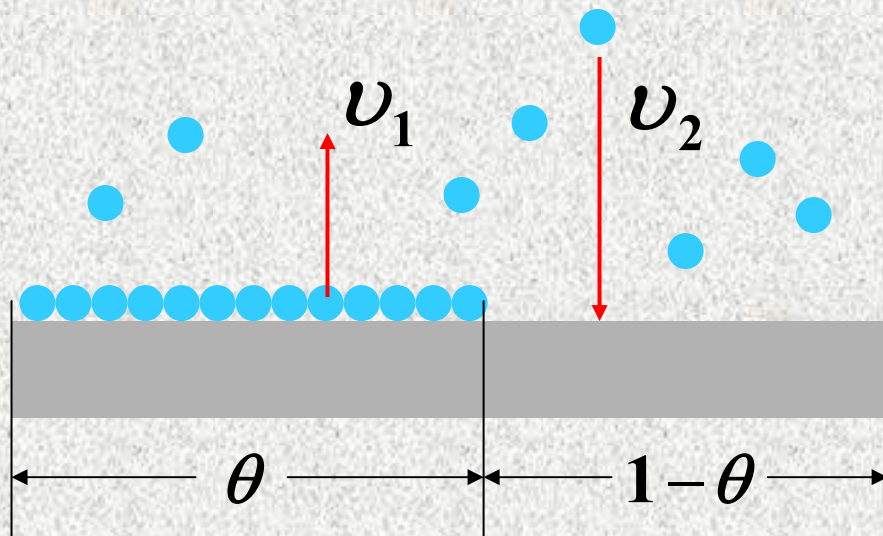
吸附系数

$$\theta = \frac{k_2 p}{k_1 + k_2 p} = \frac{bp}{1 + bp} = \frac{\Gamma}{\Gamma_\infty}$$

$$b = \frac{k_2}{k_1}$$

$$\Gamma = \Gamma_\infty \frac{bp}{1 + bp}$$

$$\frac{p}{\Gamma} = \frac{1}{\Gamma_\infty b} + \frac{p}{\Gamma_\infty}$$



$$\Gamma = \Gamma_{\infty} \frac{bp}{1+bp}$$

低压



$$bp \ll 1$$



$$1+bp \approx 1$$



$$\Gamma = \Gamma_{\infty} bp$$

高压



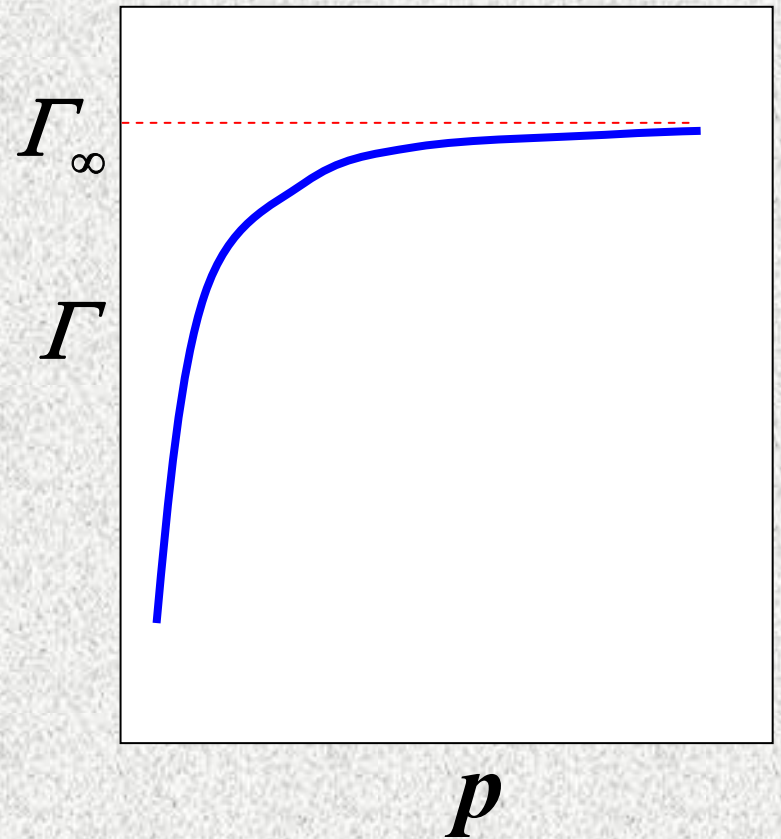
$$bp \gg 1$$



$$1+bp \approx bp$$

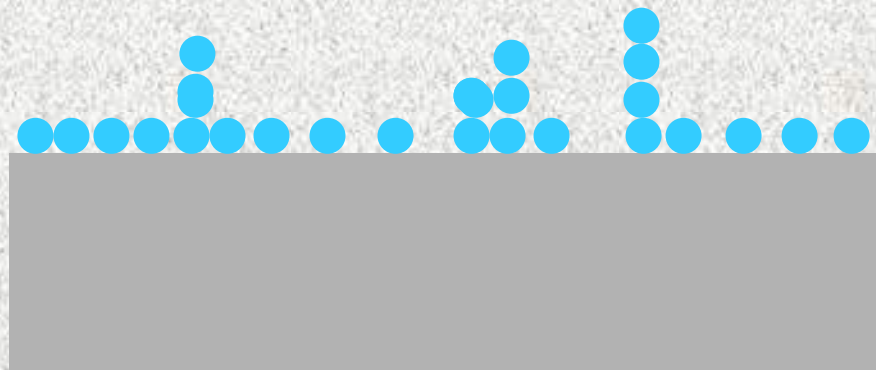


$$\Gamma = \Gamma_{\infty}$$



(3) BET吸附等温式

适用于物理吸附



$$\Gamma = \Gamma_{\infty} \frac{c p}{(p^* - p)[1 + (c - 1) p / p^*]}$$

$$\frac{p}{\Gamma(p^* - p)} = \frac{1}{\Gamma_{\infty} c} + \frac{c - 1}{\Gamma_{\infty} c} \cdot \frac{p}{p^*}$$

(4) 弗鲁姆金-斯鲁金吸附等温式

适用于非均一表面的化学吸附

$$b = A_0 \exp\left(-\frac{\Delta_{\text{ads}} H_m}{RT}\right)$$

$$\Delta_{\text{ads}} H_m = \Delta H_0 (1 - \beta\theta)$$

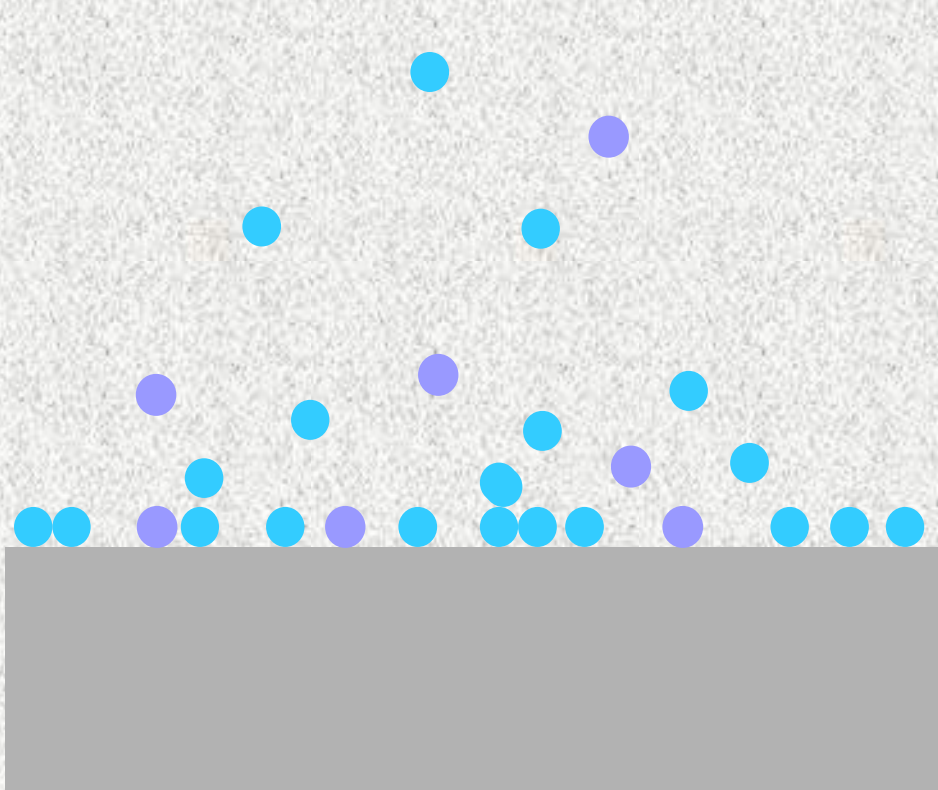
代入兰缪尔吸附等温式，令

$$A = A_0 \exp[-\Delta H_0 / (RT)]$$

$$\theta = -\frac{RT}{\beta \Delta H_0} \ln Ap$$

15-15 多相催化 动力学

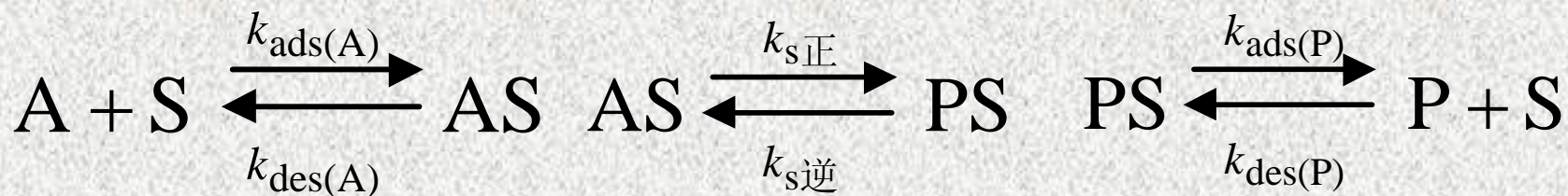
物理化学多媒体课堂教学软件 V1.0版



- ◆体相中反应物向催化剂表面扩散;
- ◆至少一种反应物被化学吸附;
- ◆表面化学反应
- ◆产物从表面解吸;
- ◆解吸产物扩散到体相中去。

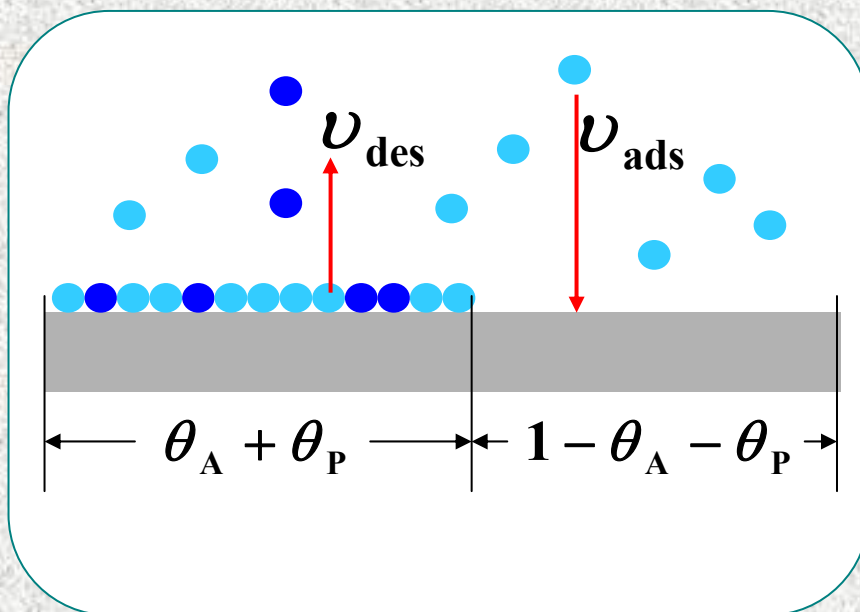
1. 扩散控制

2. 吸附或脱附控制



$$b_A = \frac{k_{\text{ads(A)}}}{k_{\text{des(A)}}}, \quad b_P = \frac{k_{\text{ads(P)}}}{k_{\text{des(P)}}$$

$$K_s = \frac{k_{\text{s正}}}{k_{\text{s逆}}}, \quad K_p = K_s \frac{b_A}{b_P}$$



设反应物A的吸附控制着整个催化反应

$$\begin{aligned}v &= k_{\text{ads(A)}} p_A (1 - \theta_A - \theta_P) - k_{\text{des(A)}} \theta_A \\ &= k_{\text{ads(A)}} p_A (1 - \theta_A - \theta_P) - k_{\text{ads(A)}} \theta_A / b_A\end{aligned}$$

设: $K_s = \theta_P / \theta_A$ $\theta_P = \frac{b_P p_P (1 - \theta_A)}{1 + b_P p_P}$

$$\theta_A = \frac{b_A p_P / K_p}{1 + b_A p_P / K_p + b_P p_P} \quad \theta_P = \frac{b_P p_P}{1 + b_A p_P / K_p + b_P p_P}$$

$$v = \frac{k_{\text{ads(A)}} (p_A - p_P / K_p)}{1 + b_A p_P / K_p + b_P p_P}$$

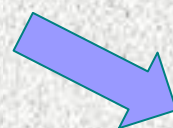
3. 界面反应控制



$$\theta_A = \frac{b_A p_A}{1 + b_A p_A + b_P p_P} \quad \theta_P = \frac{b_P p_P}{1 + b_A p_A + b_P p_P}$$

(a) 产物P的吸附可略, $b_P \approx 0$

气体A吸附很弱, $1 + b_A p_A \approx 1$



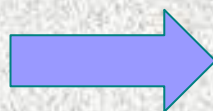
$$\theta_A = \frac{b_A p_A}{1 + b_A p_A}$$

$$v = k'_s p_A$$

气体A吸附很强, $b_A p_A \gg 1$

$$v = k_s \theta_A$$

$$\theta_A = \frac{b_A p_A}{1 + b_A p_A}$$

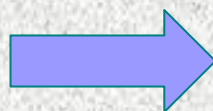


$$v = k_s$$

吸附介于强弱之间

$$v = k_s \theta_A$$

$$\theta_A = \frac{b_A p_A}{1 + b_A p_A}$$



$$v = k_s \frac{b_A p_A}{1 + b_A p_A}$$

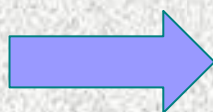


$$v = k'_s p_A^n \quad 0 < n < 1$$

(b) 反应物A的吸附很弱，产物P的吸附很强

$$b_P p_P \gg 1 + b_A p_A$$

$$\theta_A = \frac{b_A p_A}{1 + b_A p_A + b_P p_P}$$



$$\theta_A = \frac{b_A p_A}{b_P p_P}$$



$$v = k_s \theta_A$$

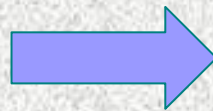
$$v = k'_s p_A / p_P$$

$$k'_s = k_s b_A / b_P$$

(c) 反应物和产物的吸附都很强

$$b_A p_A + b_P p_P \gg 1$$

$$\theta_A = \frac{b_A p_A}{1 + b_A p_A + b_P p_P}$$



$$\theta_A = \frac{b_A p_A}{b_A p_A + b_P p_P}$$



$$v = \frac{k'_s p_A}{b_A p_A + b_P p_P}$$

$$v = k_s \theta_A$$

$$k'_s = k_s b_A$$